

# Calculating phase transformations in duplex stainless steels using computational thermodynamics

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## Acknowledgment:

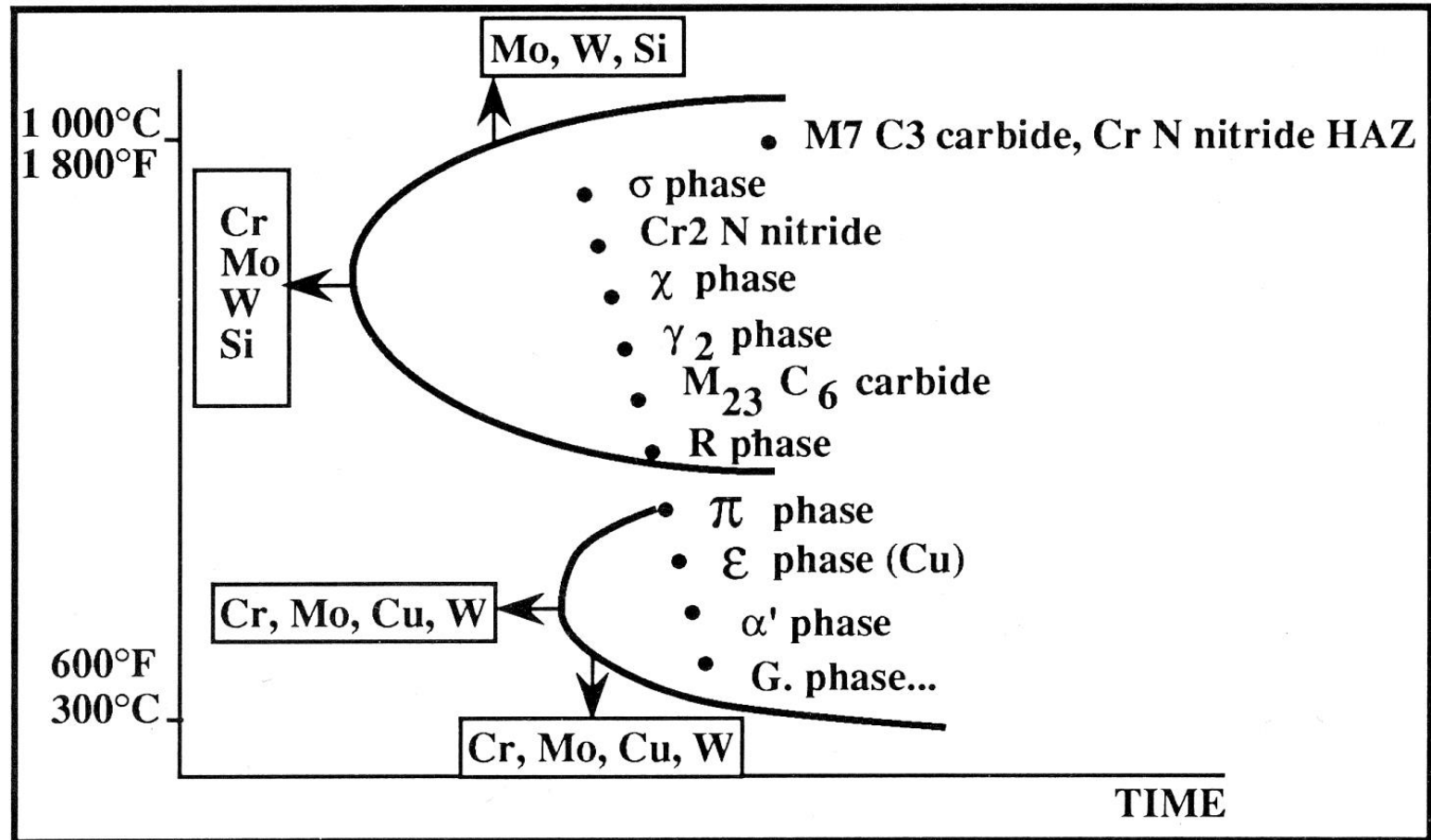
- The member research consortium MRC Stainless at Swerea KIMAB AB
- Outokumpu Stainless AB
- AB Sandvik Materials Technology
- KTH Royal Institute of Technology
- Jernkontoret - The Swedish Steel Producers' Association
- Thermo-Calc Software AB

## Duplex stainless steels:

- Consist of about equal amounts of ferrite and austenite

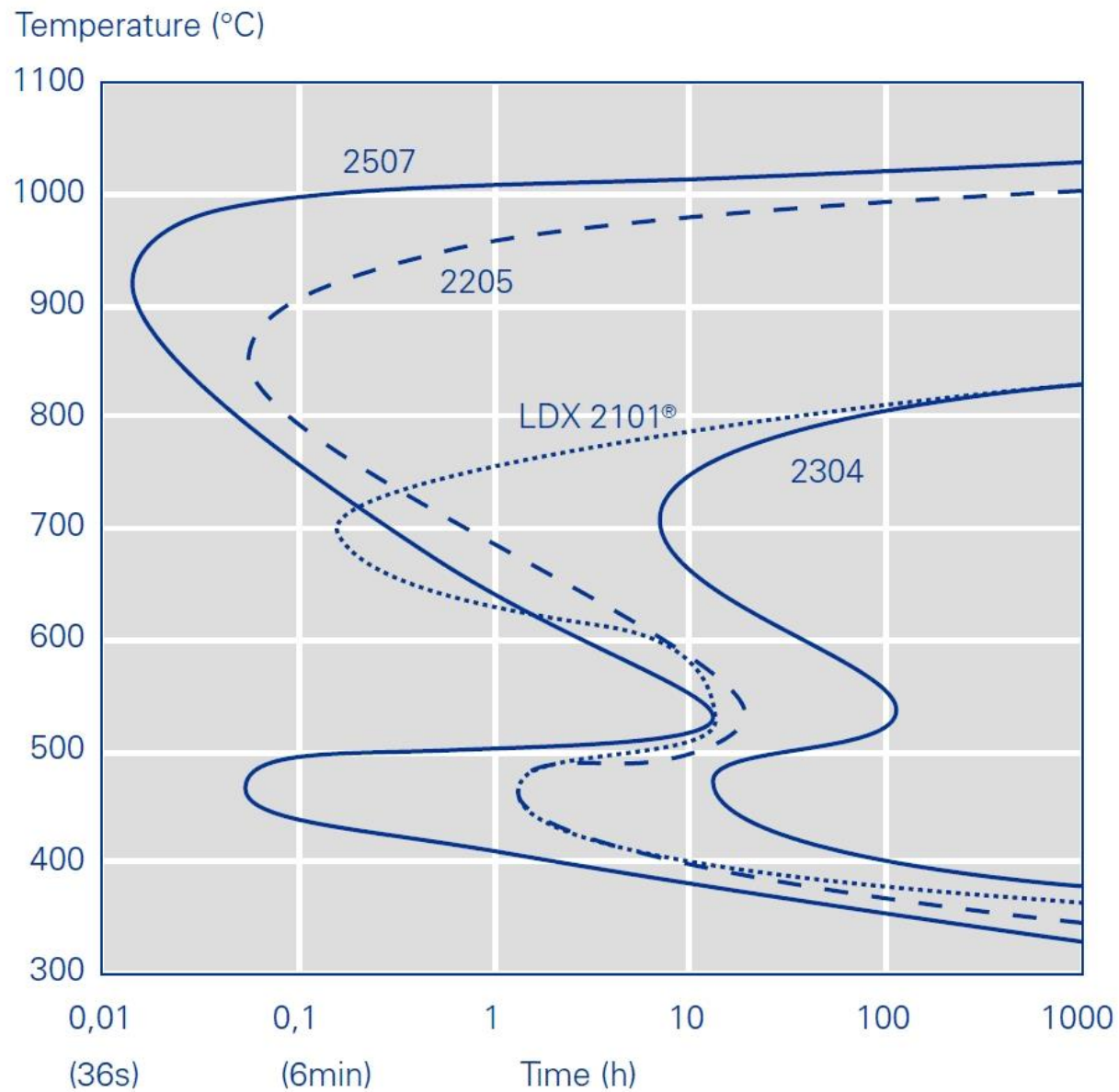
Lean: LDX 2101 <sup>®</sup>	Fe-5Mn- <b>21.5Cr</b> - <b>1.5Ni</b> -0.3Mo-0.22N
Standard: 2205	Fe- <b>22Cr</b> - <b>5.5Ni</b> -3Mo-0.17N
Super: 2507	Fe- <b>25Cr</b> - <b>7Ni</b> -4Mo-0.27N
Hyper: SAF 3207 HD <sup>™</sup>	Fe- <b>32Cr</b> - <b>7Ni</b> -3.5Mo-0.50N

- Doubled strength, compared to austenitics
  - Excellent corrosion resistance
  - Good weldability properties
  - Low Ni, compared to austenitics, i.e. favourable cost
  - Lean duplex: Ni partly substituted by Mn+N
- ☺ Cr+Mo = Corrosion resistance
- ☹ Cr+Mo = Intermetallic phases



J. Charles, Proc. Duplex Stainless Steels '91, Beaune, France, 1 (1991)

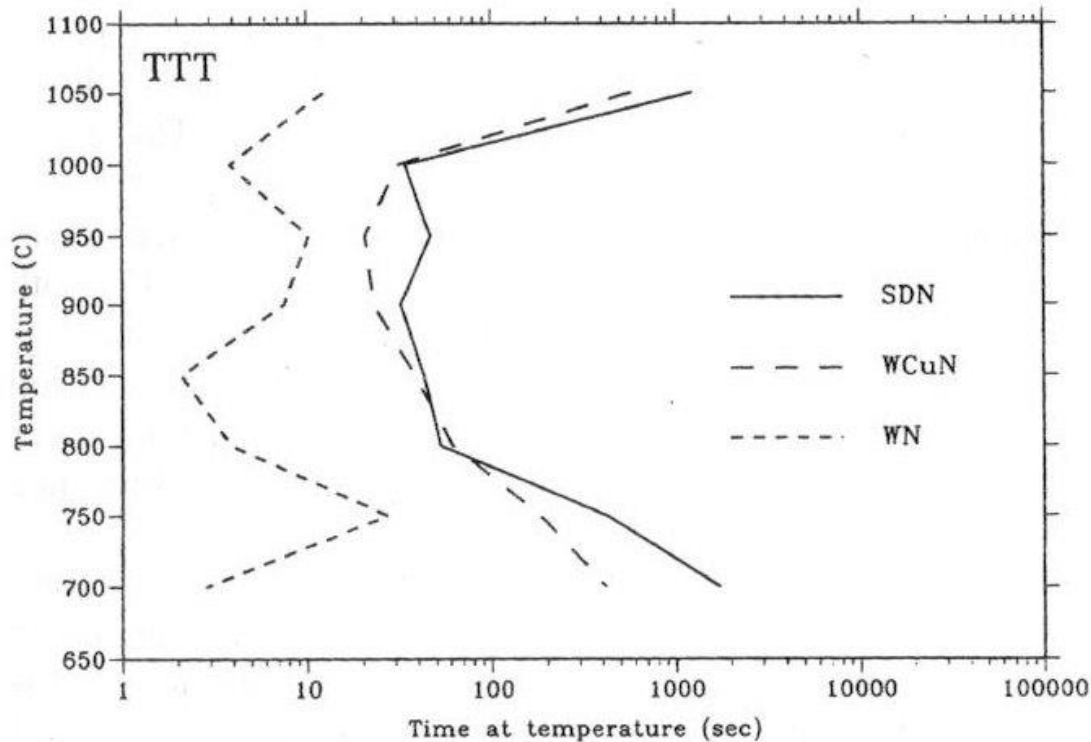
Schematic TTP (time to-precipitation) diagram



From Outokumpu Stainless AB, 50 % toughness loss

## Chemical compositions [wt.-%]:

	C	Si	Mn	Cr	Ni	Mo	N	Cu	W
<b>SDN</b>	0.034	0.75	0.72	<b>25.59</b>	<b>9.26</b>	<b>3.79</b>	<b>0.25</b>	0.09	<0.003
<b>WCuN</b>	0.038	0.38	0.93	<b>25.47</b>	<b>9.20</b>	<b>3.60</b>	<b>0.23</b>	<b>0.62</b>	<b>0.92</b>
<b>WN</b>	0.046	0.69	1.34	<b>25.67</b>	<b>9.60</b>	<b>3.09</b>	<b>0.24</b>	0.09	<b>2.34</b>



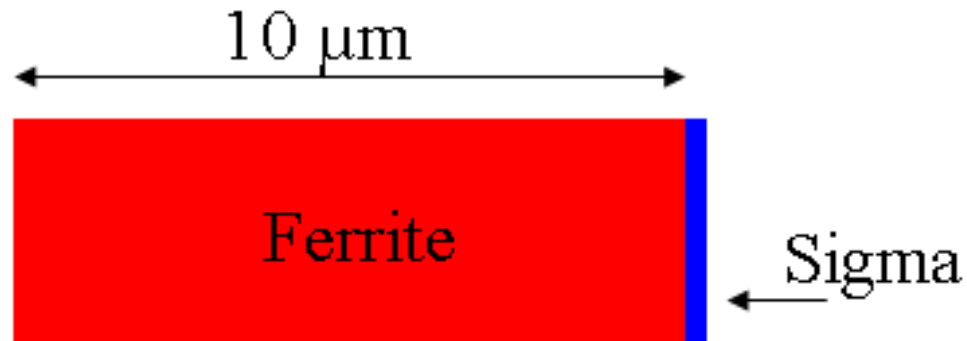
MMA welds:

- Isothermal heat treatments
- Optical microscopy
- SEM
- Point counting

TTT diagram showing C-curves representing 1 % of intermetallic phase.

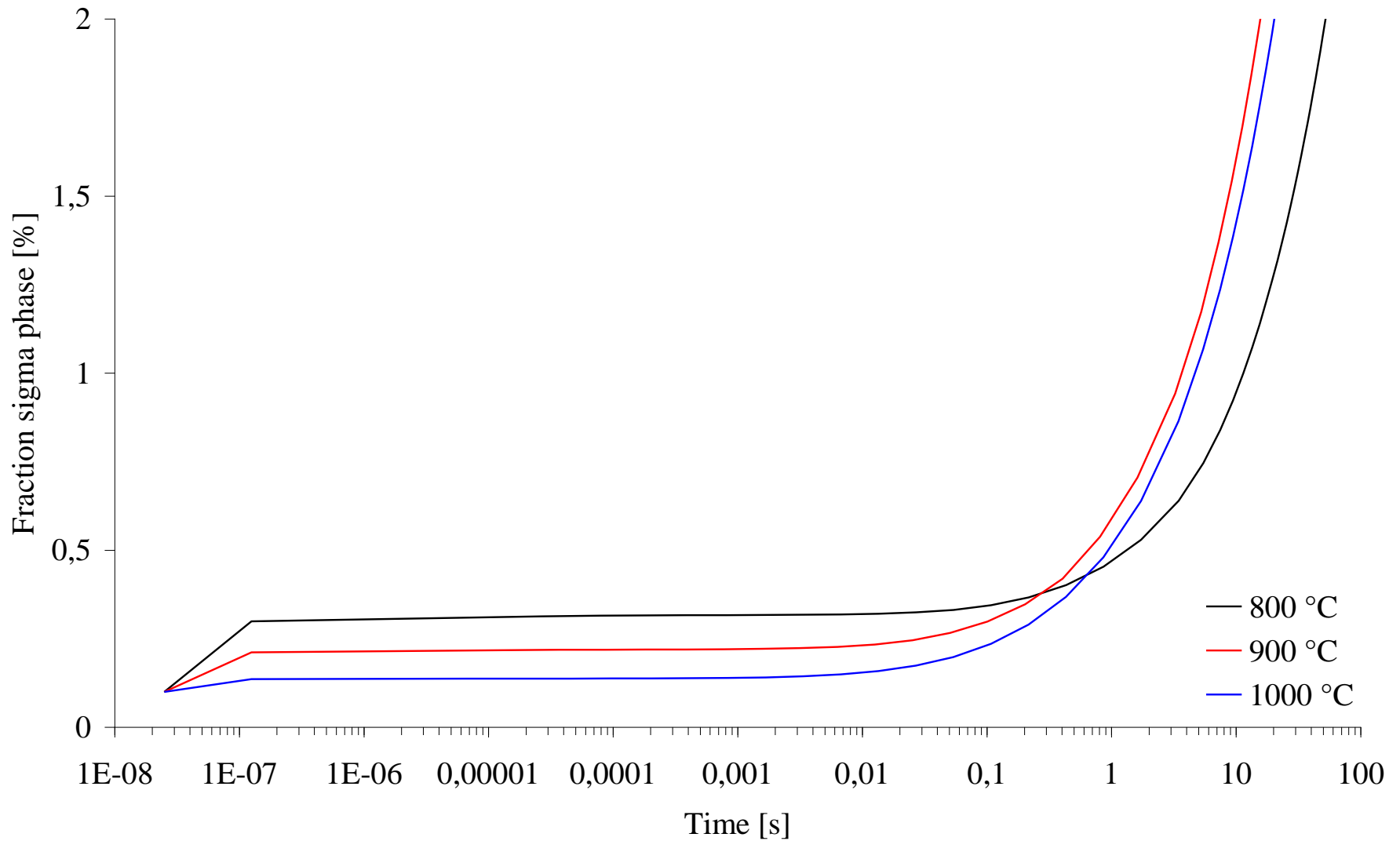
Simplified chemical compositions [wt.-%]:

	C	Si	Mn	Cr	Ni	Mo	N	Cu	W
SDN	-	-	-	25.59	9.35	3.79	0.284	-	-
WCuN	-	-	-	25.47	9.82	3.60	0.268	-	0.92
WN	-	-	-	25.67	9.69	3.09	0.286	-	2.34

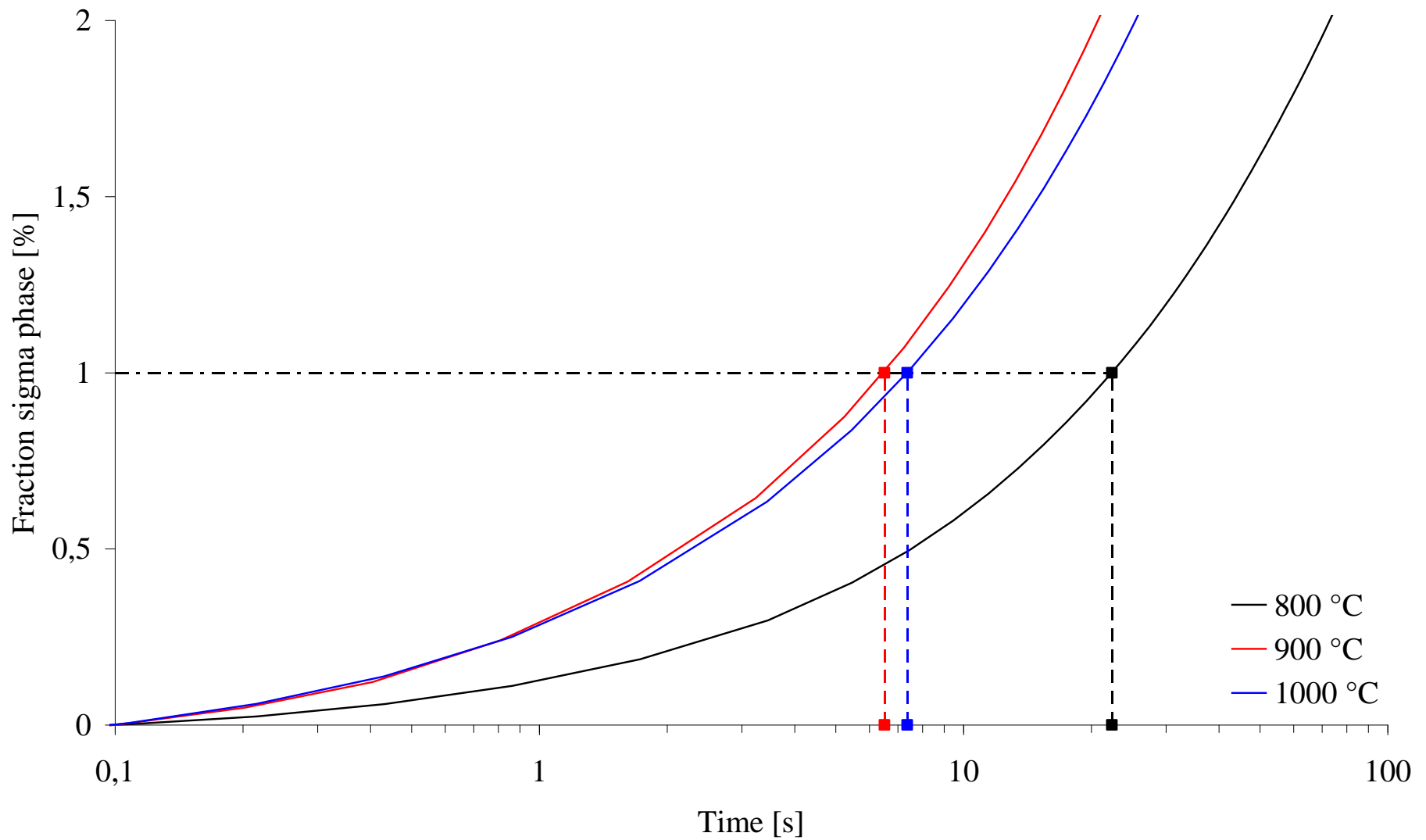


### Approach:

- Omit the austenite, only ferrite and austenite
- Simplifications: Si & Mn omitted; C  $\rightarrow$  N and Cu  $\rightarrow$  Ni
- Thermo-Calc: Calculate the ferrite composition at 1100 °C (1150 °C WN)
- 10  $\mu$ m ferrite  $\rightarrow$  DICTRA; TCFE6 & MOB1
- **Time to grow 1 % sigma phase**

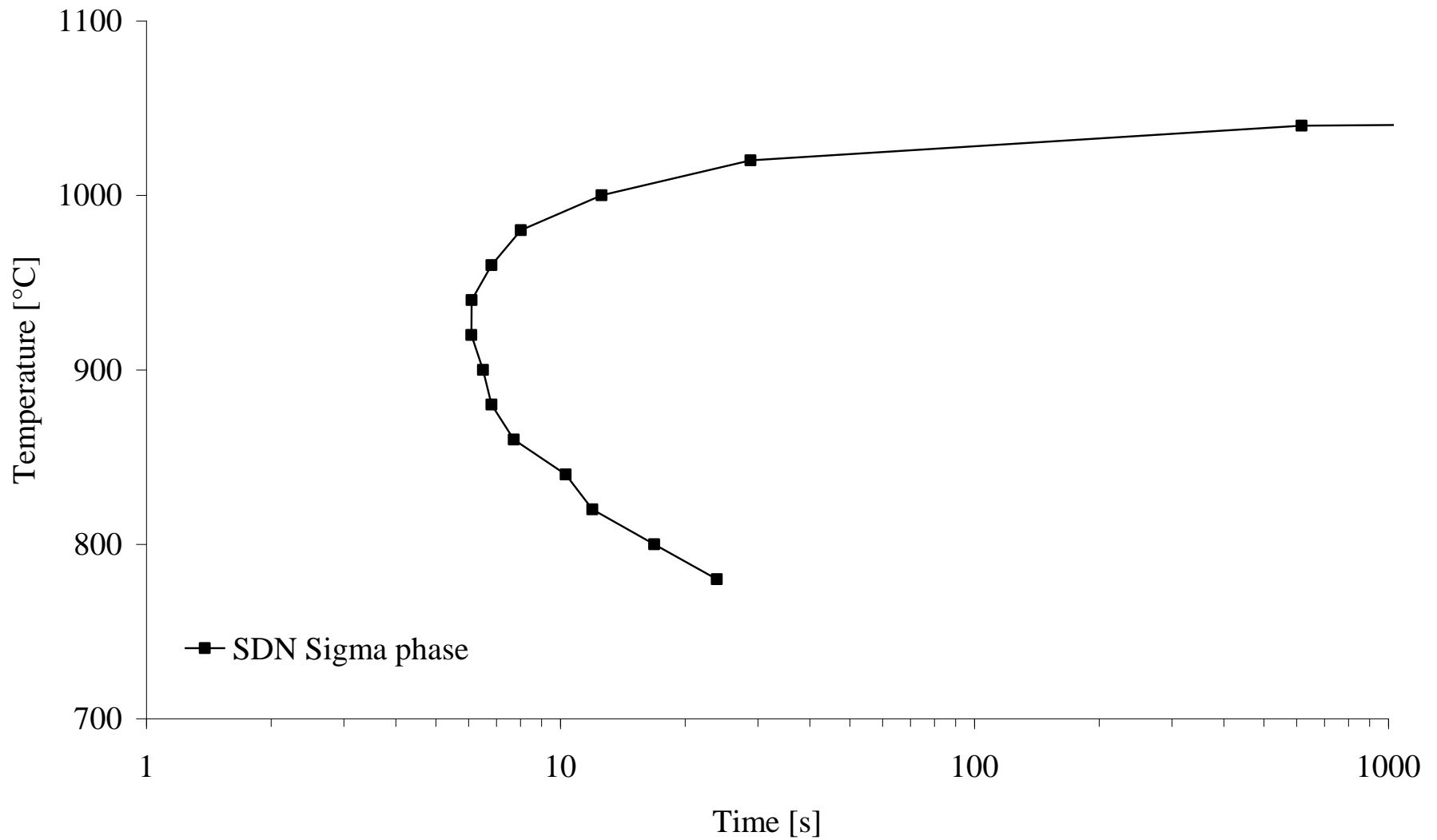


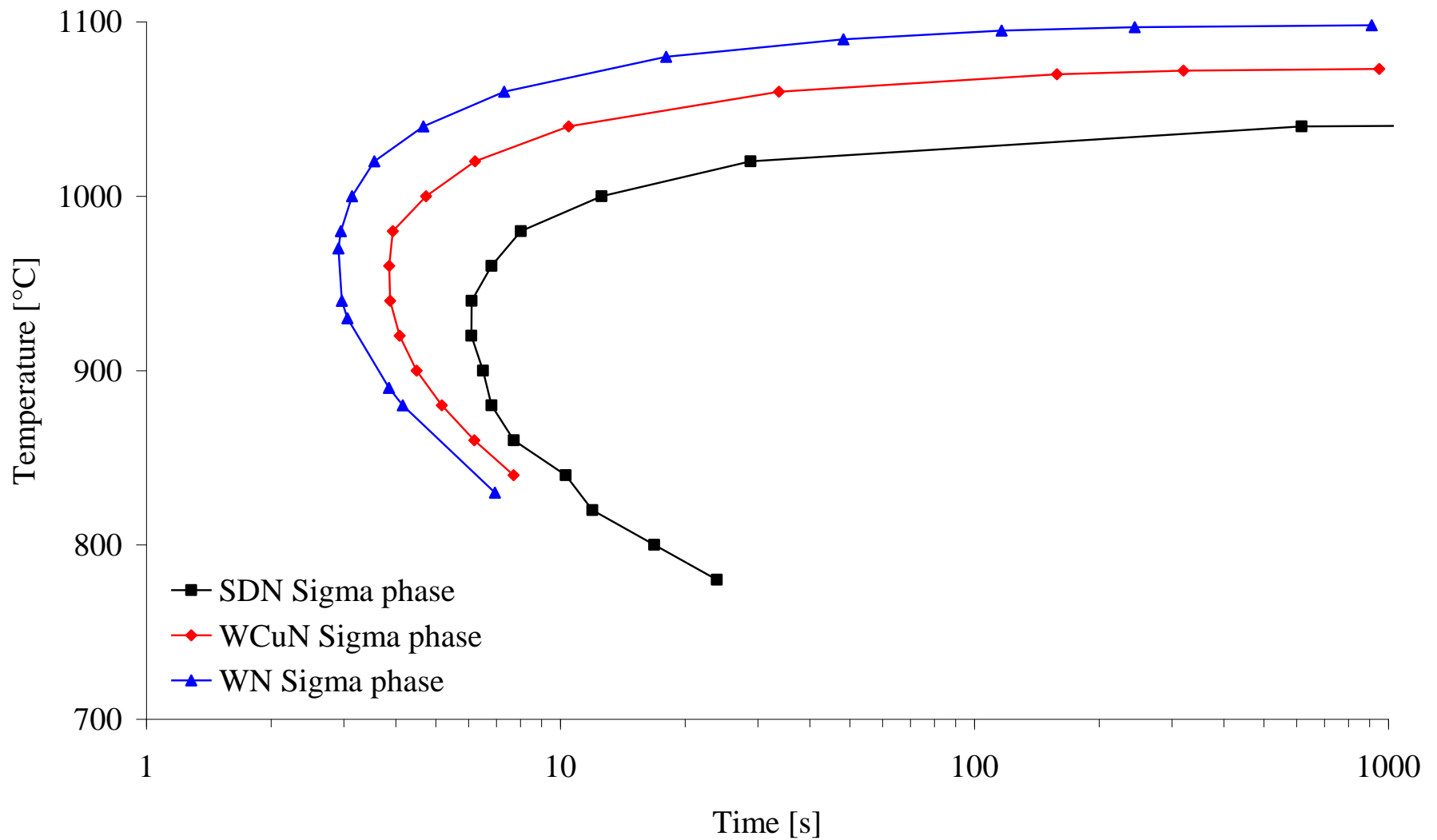
SDN: Growth of sigma phase



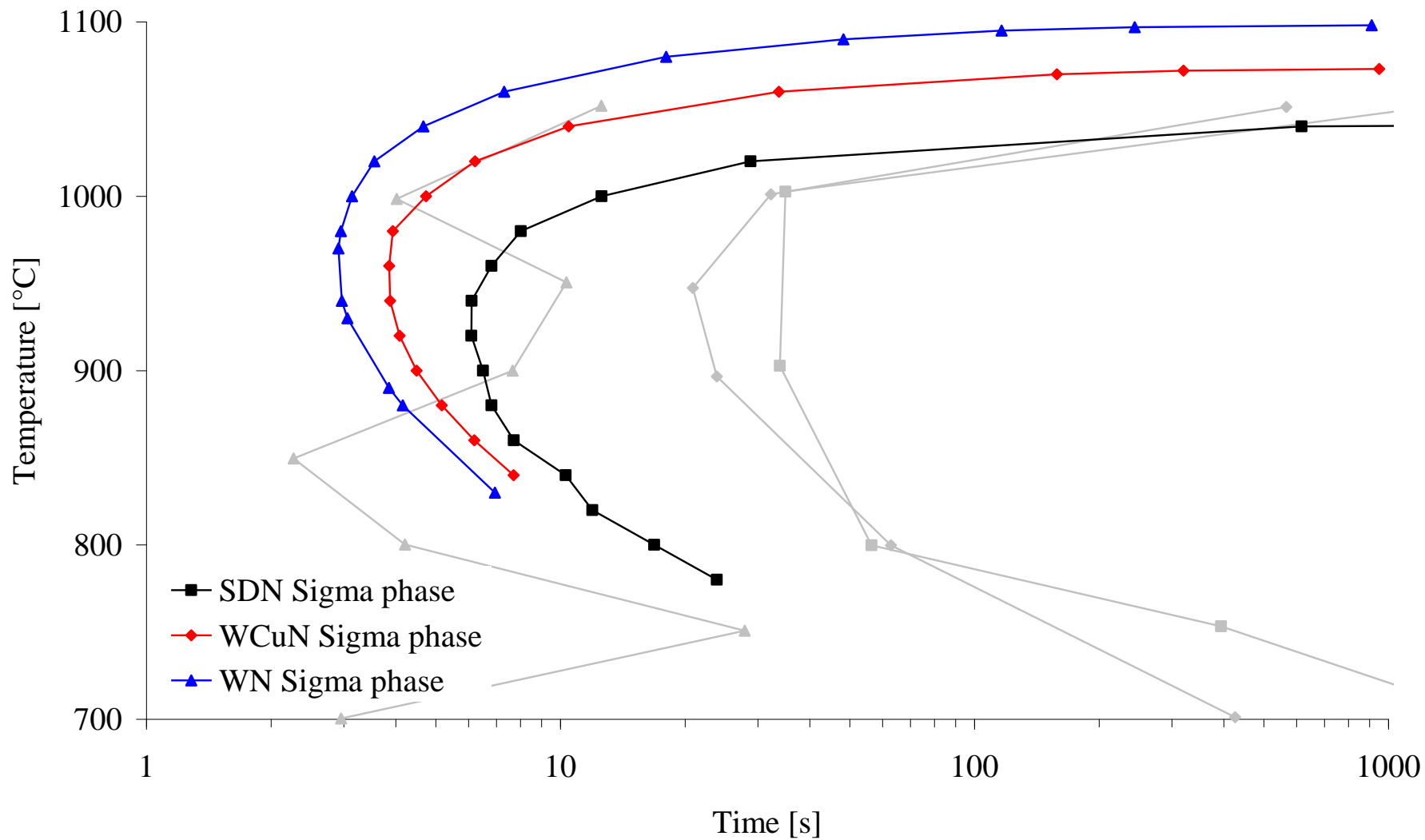
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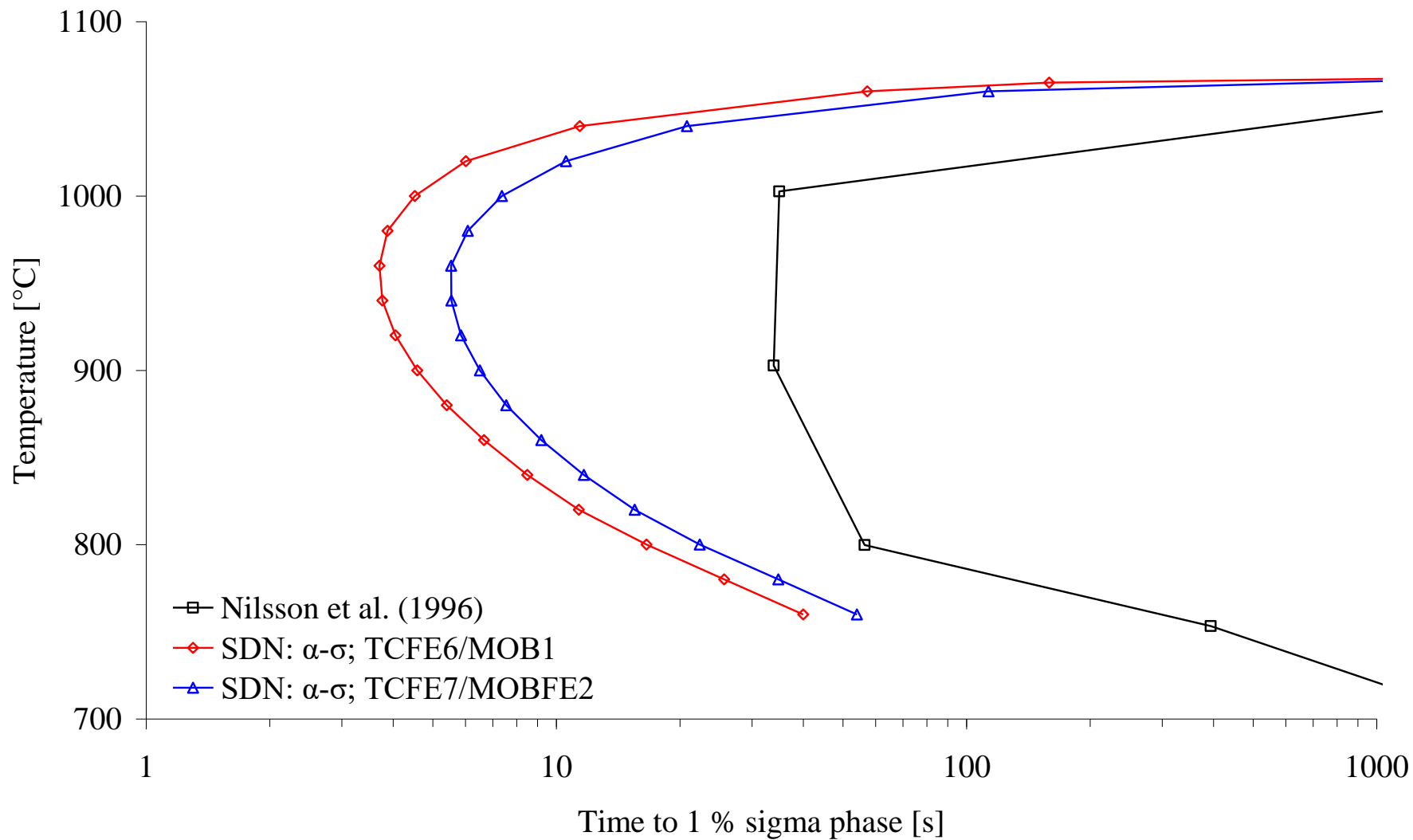




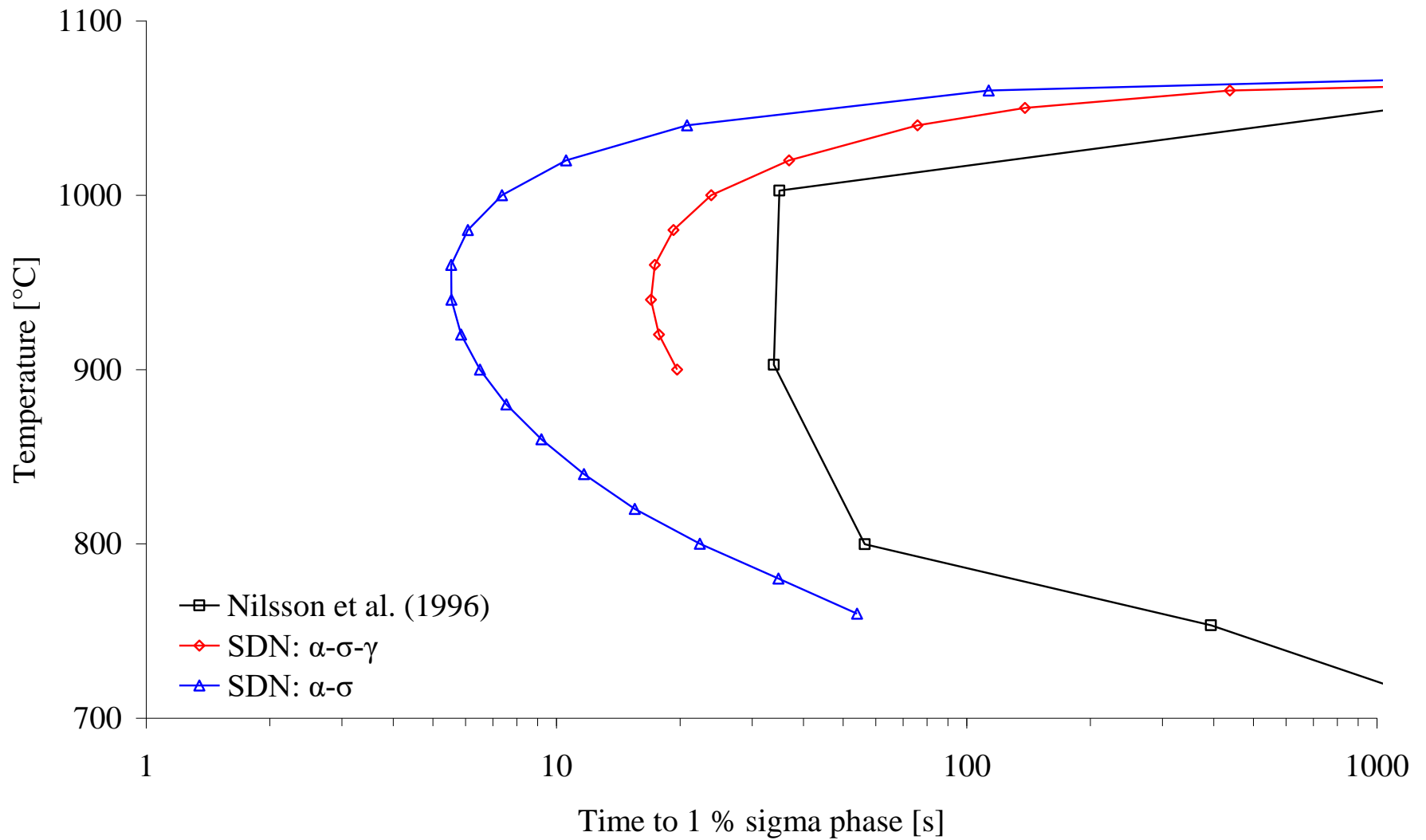
SDN, WCuN & WN: TTT-diagrams



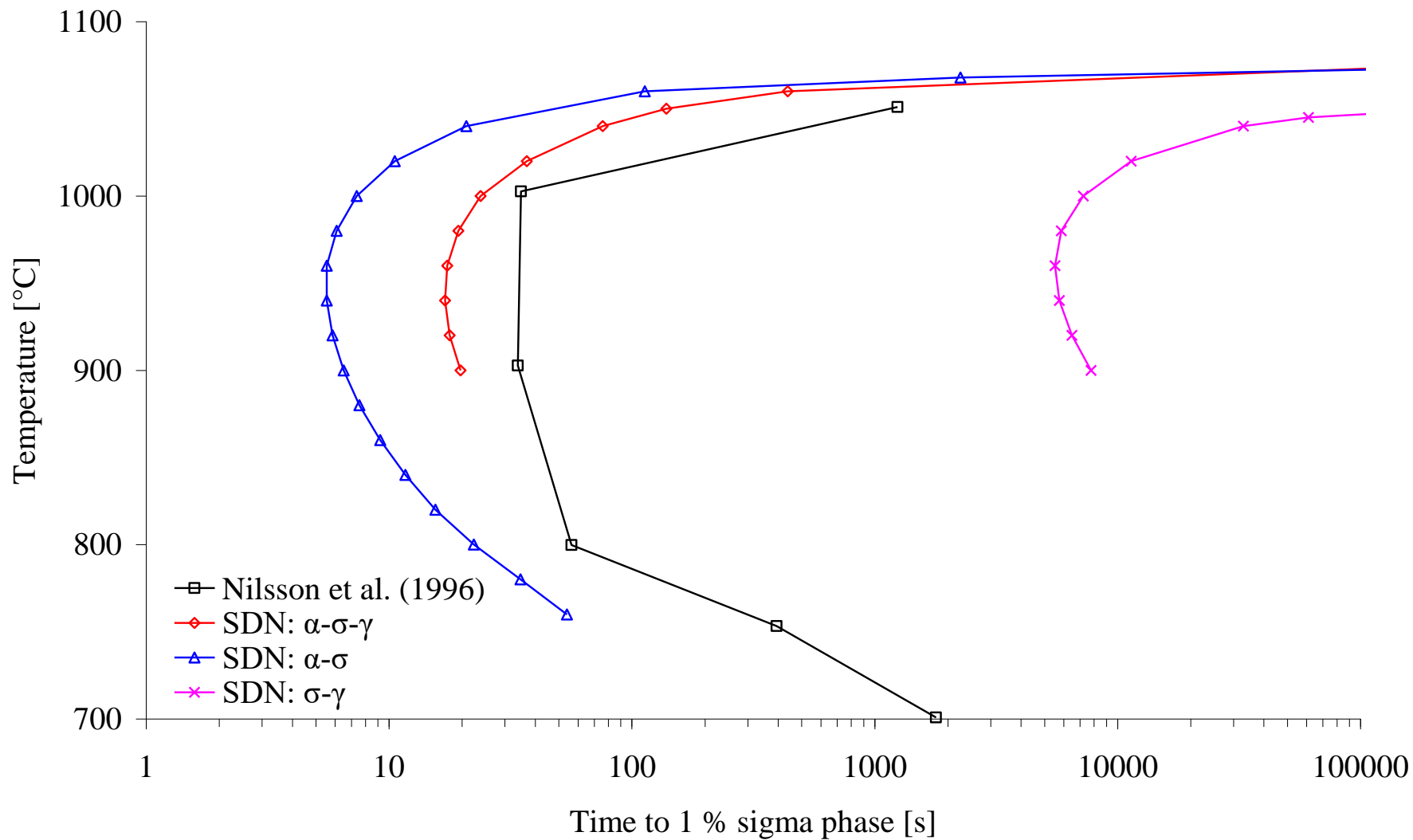
SDN, WCuN & WN: TTT-diagrams



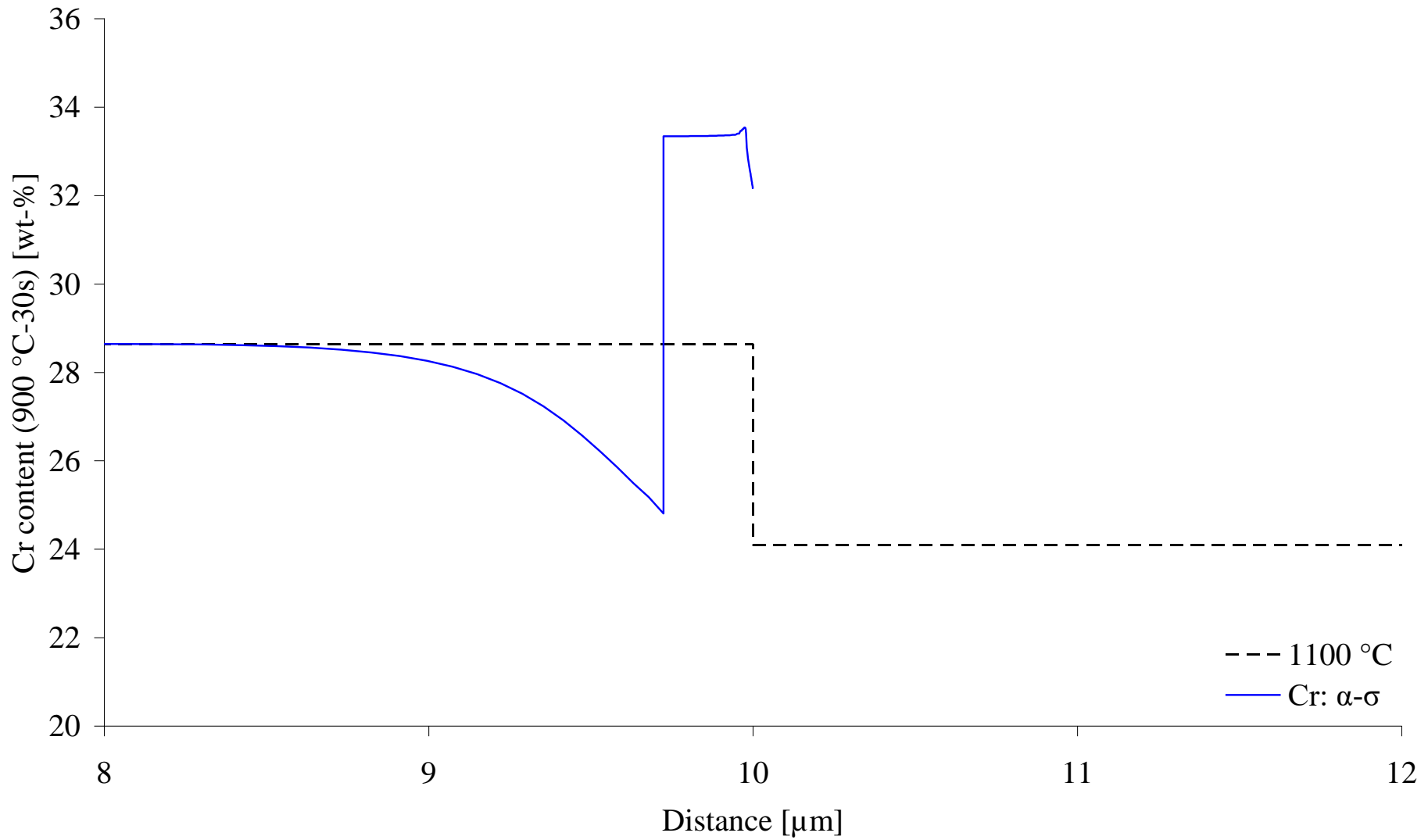
SDN: TCFE6/MOB1 & TCFE7/MOBFE2



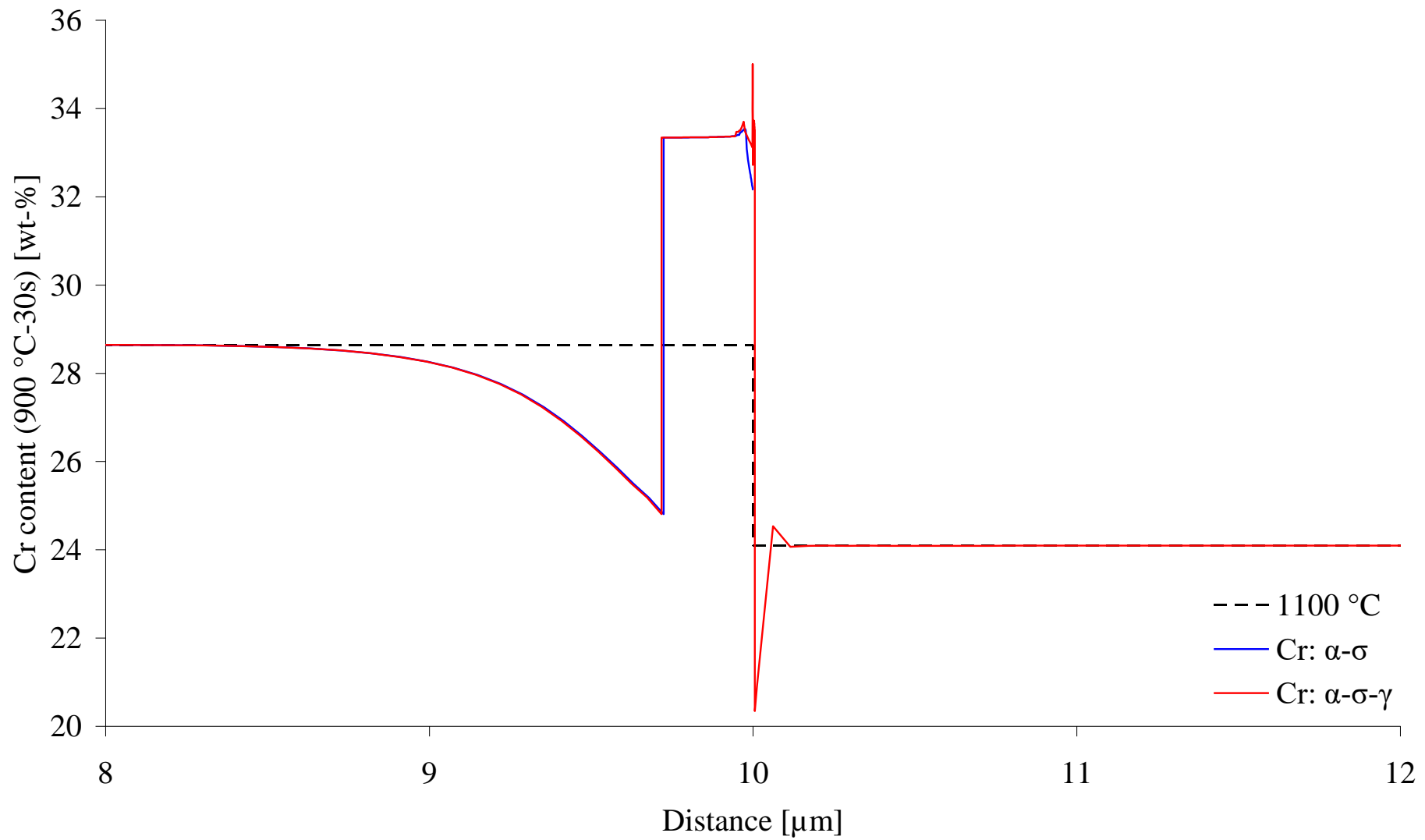
SDN:  $\alpha$ - $\sigma$ - $\gamma$  versus  $\alpha$ - $\sigma$



SDN:  $\alpha$ - $\sigma$ - $\gamma$  &  $\alpha$ - $\sigma$  versus  $\sigma$ - $\gamma$

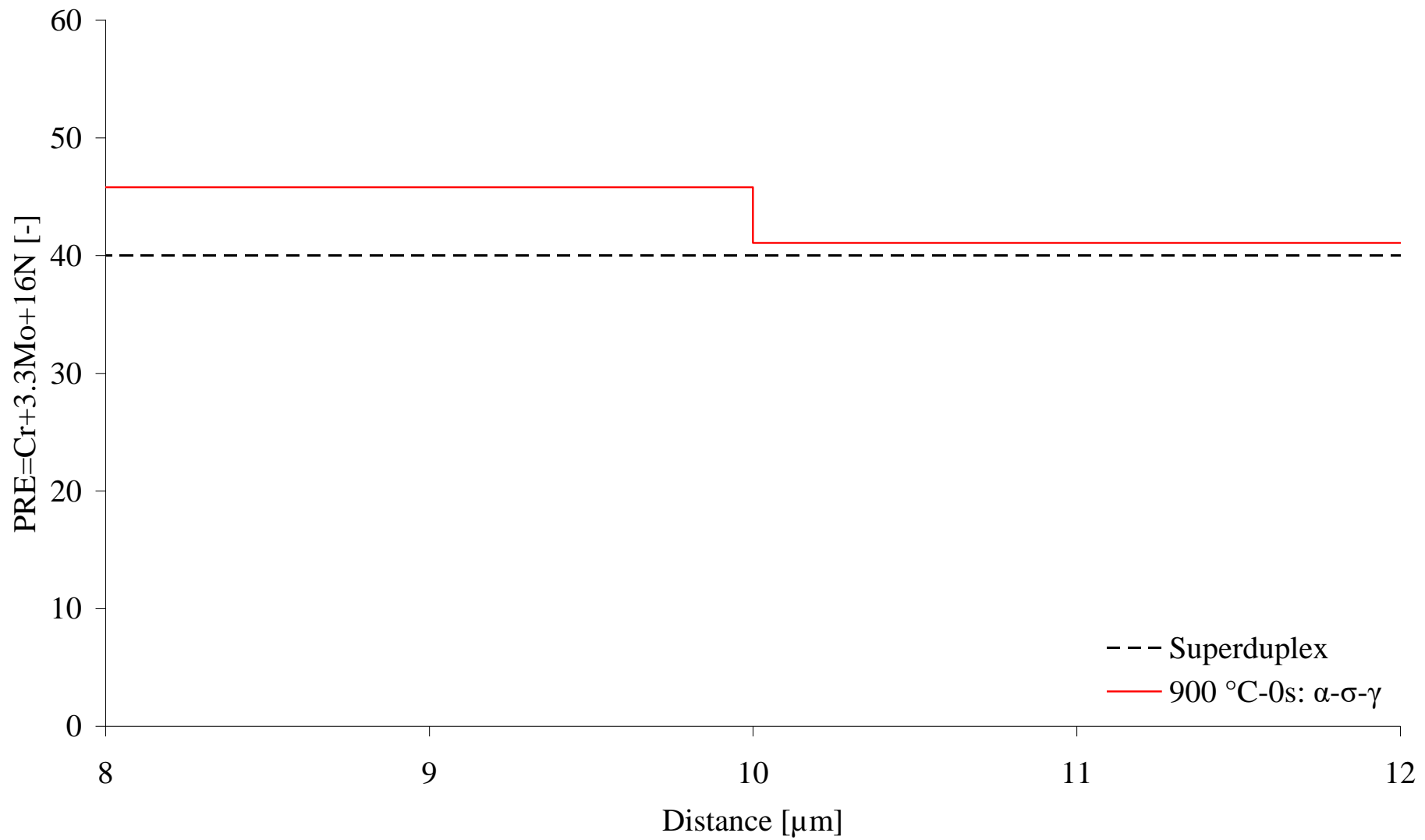


SDN: Depleted zones, 900 °C-30 s

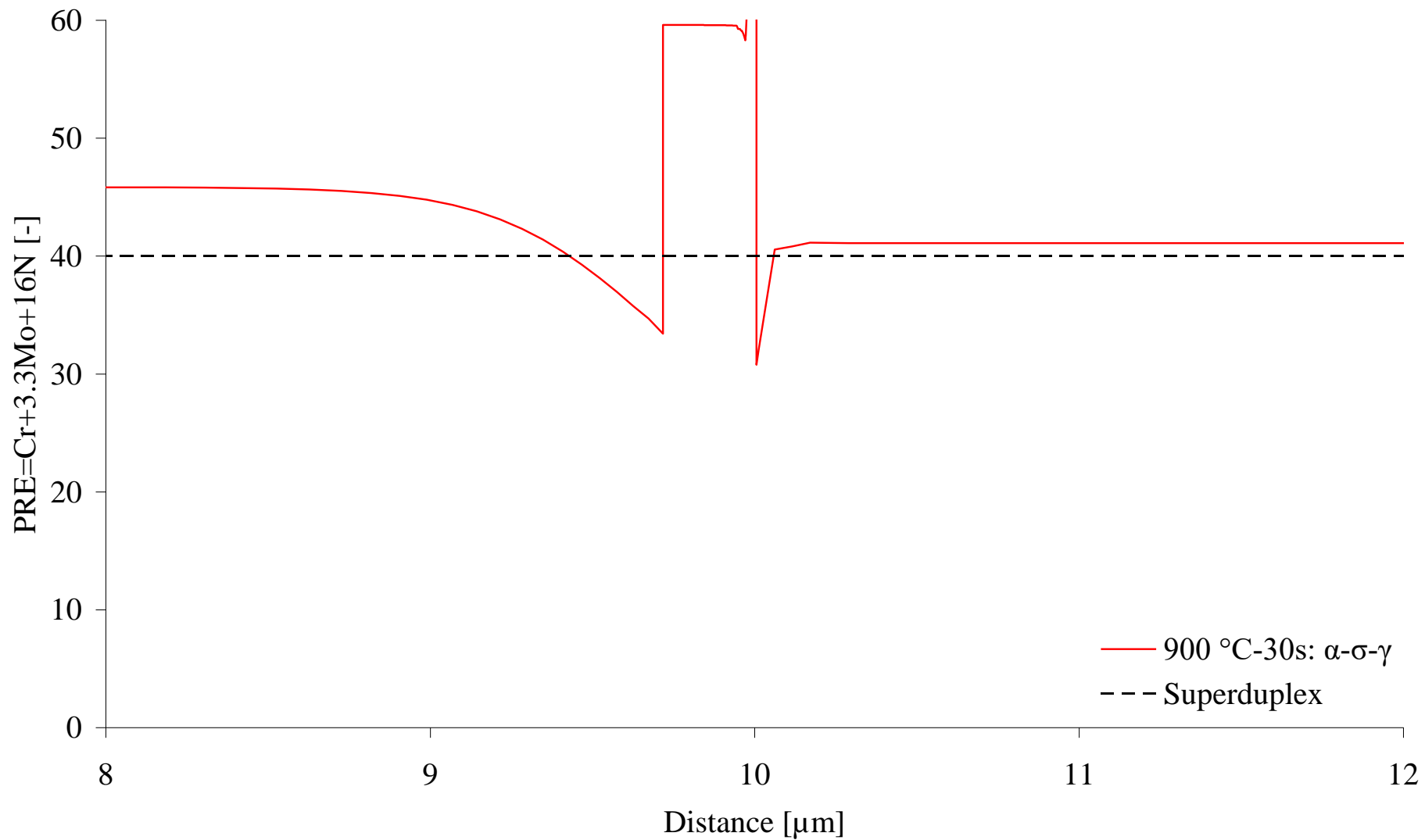


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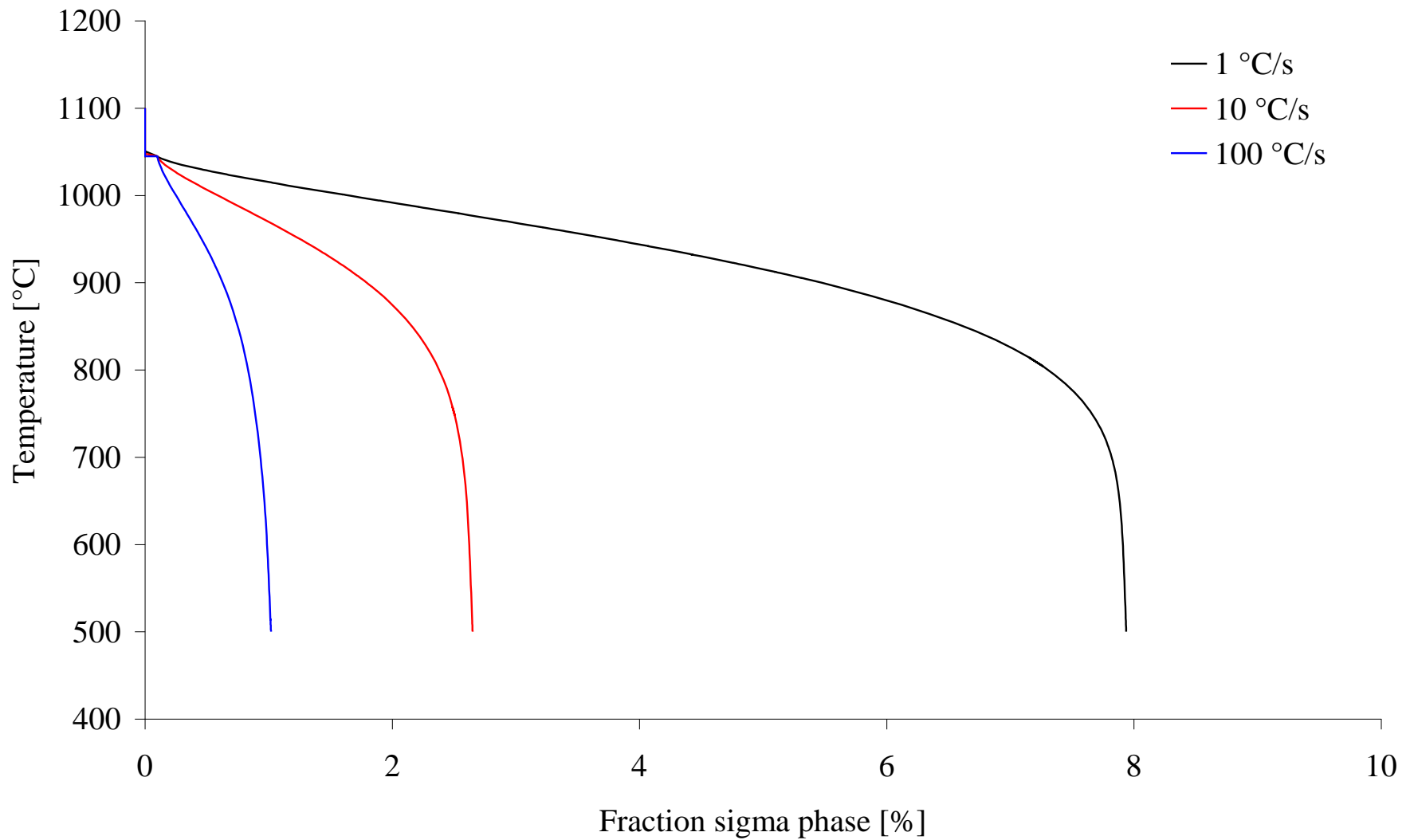


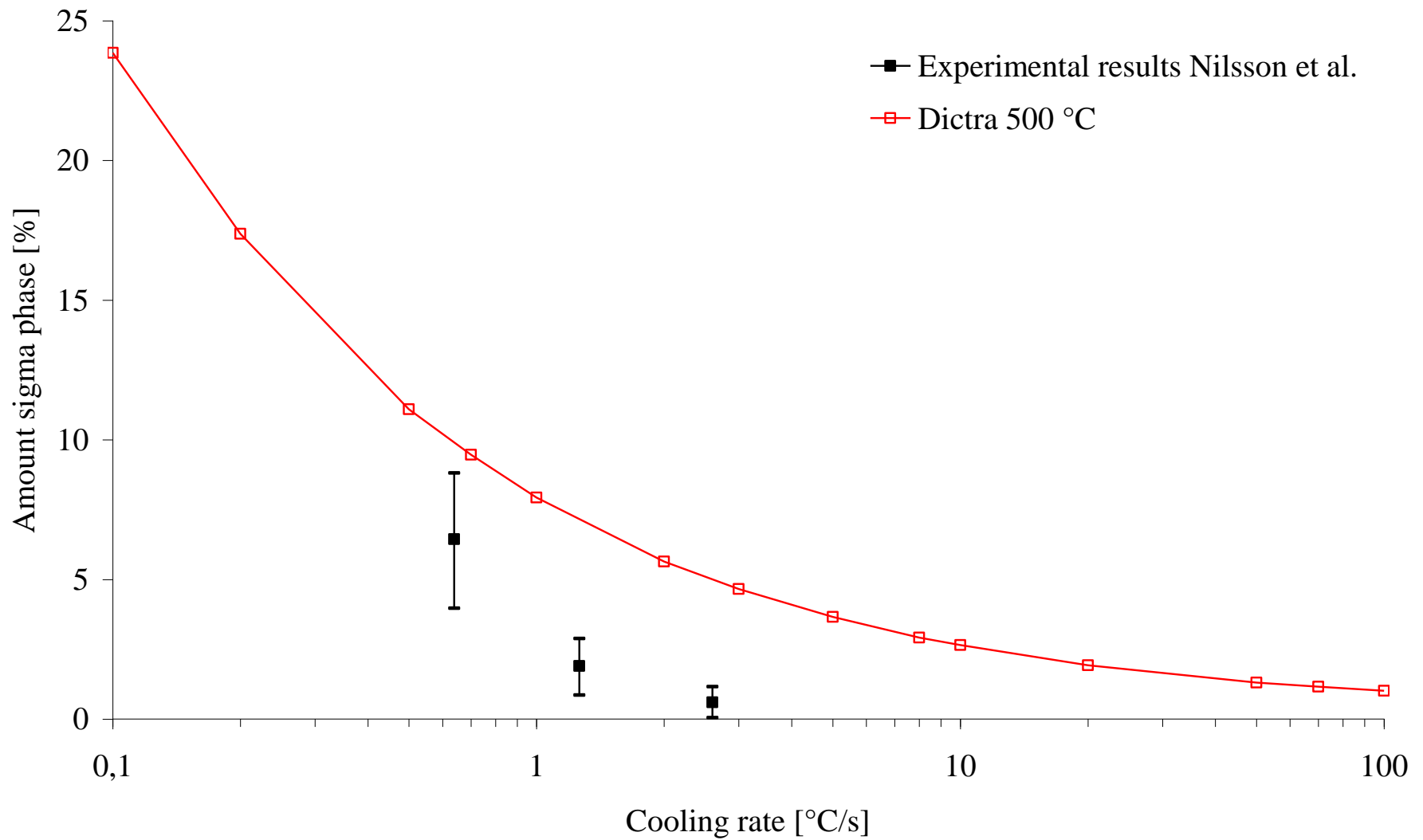


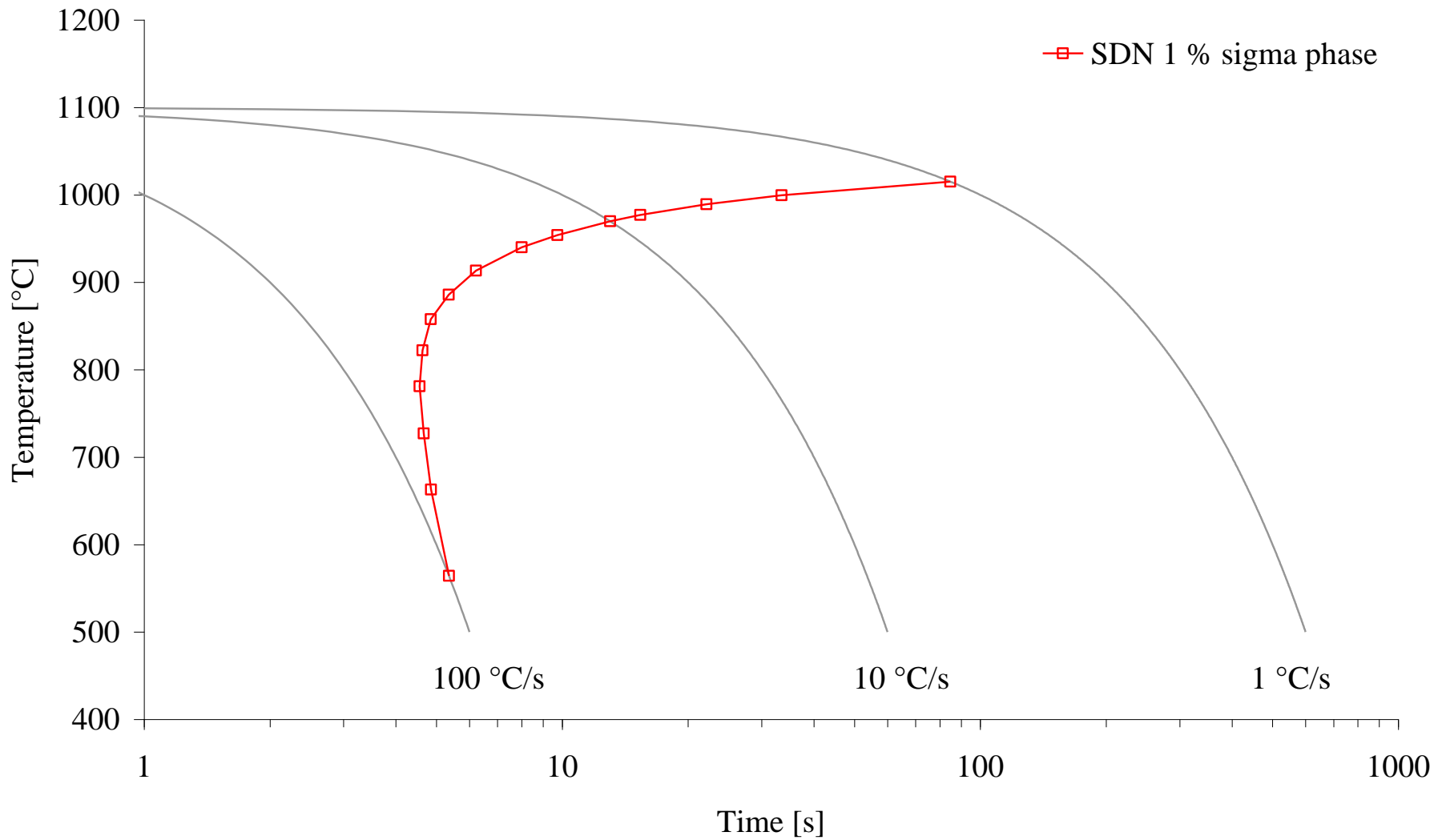
SDN: Pitting resistance equivalent  $PRE = Cr + 3.3Mo + 16N$



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## Conclusions:

- DICTRA can be used successfully to reproduce TTT and CCT diagrams.
- Growth of depleted zones adjacent to secondary phases can be studied.
- The influence of alloy composition on precipitation and growth kinetics of intermetallic phases can be derived.
- A good theoretical reproduction of tedious experimental and metallographic work was achieved.
- An extension with nominal compositions gave further insight to the influence of the individual elements W and Cu.

## Critical issues :

- Austenite phase was omitted for sake of simplicity.
- Multiple phases was not considered, but the intermetallics one by one.
- Cell size is a **very** critical parameter !
- Nucleation was omitted, by good reason ?

*S. Wessman, R. Pettersson: Application of computational thermodynamics to predict growth of intermetallic phases in superduplex stainless steels, Steel Research International 86 (2015).*