

# Graphical Mode Examples Guide

Thermo-Calc Version 2018a



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## About the Graphical Mode Examples

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Graphical Mode examples are available for Thermo-Calc and the add-on Diffusion Module (DICTRA) and Precipitation Module (TC-PRISMA). These are in the format of project files (\*.tcu).



Also search the online help for "Opening Graphical Mode Project Files", which is in the *Thermo-Calc User Guide*.

This guide includes the example descriptions and information about how to open a Graphical Mode *project* file.

## Watch the Video Tutorials

Many of the Graphical Mode examples have video tutorials available both on [our website](#) and our [YouTube channel](#).

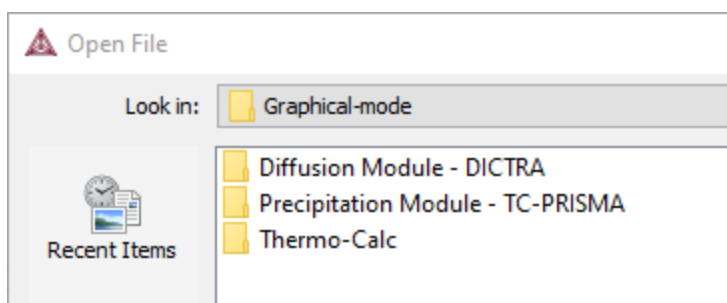


You can go to the video tutorials when in Thermo-Calc: **Help → Video Tutorials**.

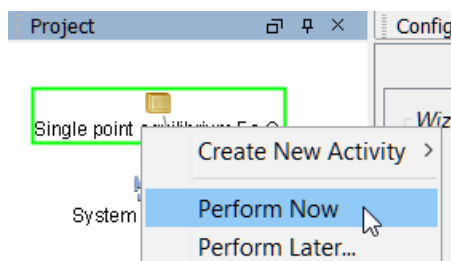
## Opening a Project File

To open an example project file for Thermo-Calc and the add-on Diffusion Module (DICTRA) and/or Precipitation Module (TC-PRISMA):

1. Open Thermo-Calc.
2. Confirm you are in Graphical Mode. If not, click the **Switch to Graphical Mode** button.
3. From the main menu, select **File →** or **Help → Examples Files**.
4. The examples are divided into folders by product (the add-on Diffusion Module (DICTRA) and/or Precipitation Module (TC-PRISMA) and Thermo-Calc). Navigate to the folder and project file you want and double-click to open.



5. The Graphical Mode examples are stored without calculated results so you will want to run the example calculation and generate a plot or table. To do this, click the first node in the tree at the top of the **Project** window. Then right-click and select **Perform now**.



Some add-on module examples require additional licenses to run for more than three elements.

## Thermo-Calc Graphical Mode Examples

This guide includes descriptions of the following examples.

Category	Example number
Thermo-Calc including binary and ternary system examples, Scheil, and the Property Model and Equilibrium Calculators plus more	T_01 to T_12
Diffusion Calculator Examples	D_01, D_02, D_03 (the Quick Start Guide Examples) D_04 to D_07
Precipitation Calculator Examples	P_01 to P_11

### *T\_01: Calculating a Single-Point Equilibrium*

This example shows the result from a single-point equilibrium calculation in the Fe-C system. It demonstrates the use of the Equilibrium Calculator and generates a Table Renderer in the **Results** window. The number of equilibrium conditions is C+2 where C is the number of components, meaning that four conditions are needed in this example:

- **Temperature** is 1000 K
- **Pressure** is 101325 Pa
- **System size** is 1 mole
- **Mass percent carbon** is 0.1%

### PROJECT FILE AND VIDEO TUTORIAL INFORMATION

- Folder: Thermo-Calc
- File name: *T\_01\_Single-point\_equilibrium.tcu*
- This example is included in the tutorial on our [website](#) and [YouTube](#) channel.

## TABLE RESULT

The displayed results of the calculation show that the BCC\_A2 (ferrite) and GRAPHITE phases are stable for this set of equilibrium conditions.

Results				
Table Renderer 1				
<b>System</b>				
Moles	1.00000			
Mass	55.64392	[g]		
Temperature	1000.00000	[K]		
Total Gibbs Energy	-42141.28527	[J]		
Enthalpy	24706.54116	[J]		
Volume	7.30619E-6	[m3]		
<i>Component</i>	<i>Mole Fraction</i>	<i>Mass Fraction</i>	<i>Activity</i>	<i>Potential</i>
C	0.00463	0.00100	0.21816	-12658.89428
Fe	0.99537	0.99900	0.00619	-42278.50542
<b>Stable Phases</b>				
	<i>Moles</i>	<i>Mass</i>	<i>Volume Fraction</i>	
<b>BCC_A2#1</b>	0.99609	55.59692	0.99711	Composition ▾
<b>Composition</b>				
<i>Component</i>	<i>Mole Fraction</i>	<i>Mass Fraction</i>		
Fe	0.99928	0.99984		
C	0.00072	0.00016		
	<i>Moles</i>	<i>Mass</i>	<i>Volume Fraction</i>	
<b>GRAPHITE#1</b>	0.00391	0.04700	0.00289	Composition ▾
<b>Composition</b>				
<i>Component</i>	<i>Mole Fraction</i>	<i>Mass Fraction</i>		
C	1.00000	1.00000		
Fe	0.00000	0.00000		

### *T\_02: Stepping in Temperature in the Fe-C System*

This example shows how the fractions of stable phases vary for an Fe-0.1 mass-% C alloy when the temperature is varied between 500 and 2000 K. It demonstrates the use of the Equilibrium Calculator. To allow temperature to vary, the corresponding **Axis Definition** check box is selected.

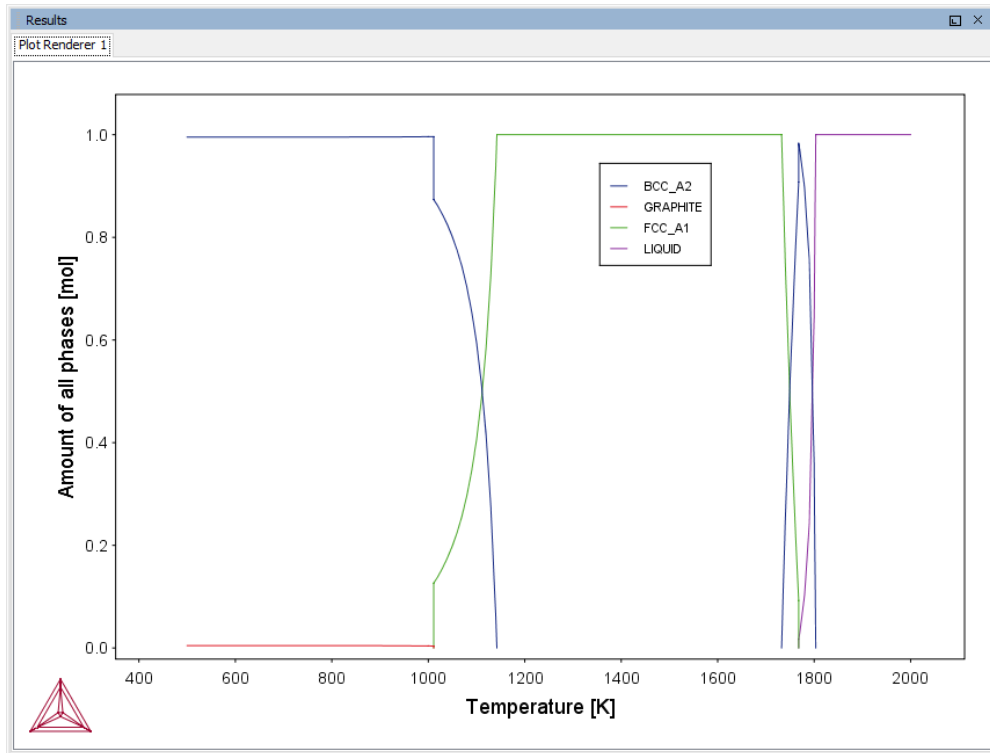
### PROJECT FILE AND VIDEO TUTORIAL INFORMATION

- Folder: Thermo-Calc
- File name: *T\_02\_Step\_in\_temperature\_in\_Fe-C.tcu*
- This example is included in the tutorial on our [website](#) and [YouTube](#) channel.



## PLOT RESULT

In this example, results are displayed graphically using a Plot Renderer activity.



If you want, you can use a Table Renderer to generate text results instead, as shown in this example after adding a Table Renderer to the Equilibrium Calculator and clicking **Perform**.

Results				
Plot Renderer 1 Table Renderer 1				
Temperature [K]	Amount of BCC_A2 [mol]	Amount of FCC_A1 [mol]	Amount of GRAPHITE [mol]	Amount of LIQUID [mol]
1000.00000	0.99609		0.00391	
1010.00000	0.99618		0.00382	
1011.17630	0.99620		0.00380	
1011.17630	0.99620	0.00000	0.00380	
1011.17630	0.87367	0.12633	0.00000	
1011.17630	0.87367	0.12633		
1020.00000	0.86050	0.13950		
1030.00000	0.84335	0.15665		
1040.00000	0.82359	0.17641		
1050.00000	0.80085	0.19915		
1060.00000	0.77399	0.22601		
1070.00000	0.74184	0.25816		
1080.00000	0.70282	0.29718		
1090.00000	0.65470	0.34530		
1100.00000	0.59418	0.40582		
1110.00000	0.51618	0.48382		
1120.00000	0.41250	0.58750		
1130.00000	0.26894	0.73106		
1140.00000	0.05863	0.94137		
1142.15538	0.00000	1.00000		
1142.15538		1.00000		
1150.00000		1.00000		
1160.00000		1.00000		
1170.00000		1.00000		
1180.00000		1.00000		
1190.00000		1.00000		
1200.00000		1.00000		
1210.00000		1.00000		
1220.00000		1.00000		

### T\_03: Fe-C Phase Diagrams

This example shows the stable Fe-C phase diagram (stable meaning that the graphite phase is entered in the calculation). The same diagram is calculated using the Binary Calculator activity and then using a System Definer and Equilibrium Calculator.

In both cases, a Plot Renderer is used to display results. The purpose of the Binary Calculator is to simplify common calculations for binary systems. In the Equilibrium Calculator two axes are defined: *Mass percent C* and *Temperature*. An axis variable must also be an equilibrium condition.

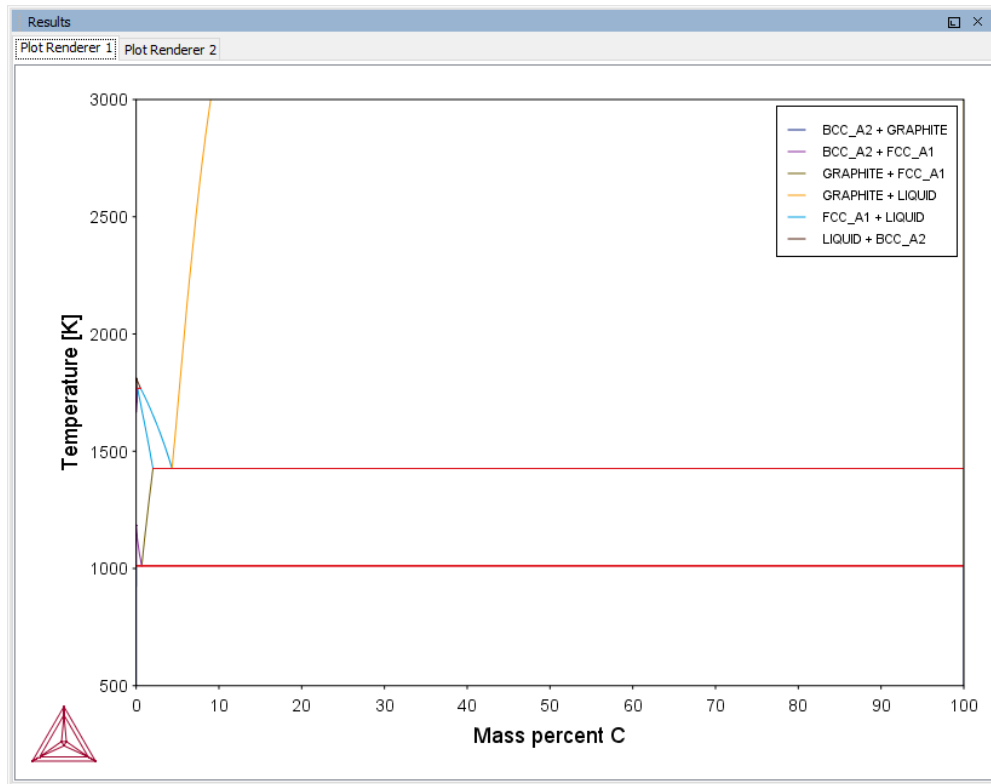
### PROJECT FILE AND VIDEO TUTORIAL INFORMATION

- Folder: Thermo-Calc
- File name: *T\_03\_Fe-C\_phase\_diagram.tcu*
- This example is included in the tutorial on our [website](#) and our [YouTube](#) channel.

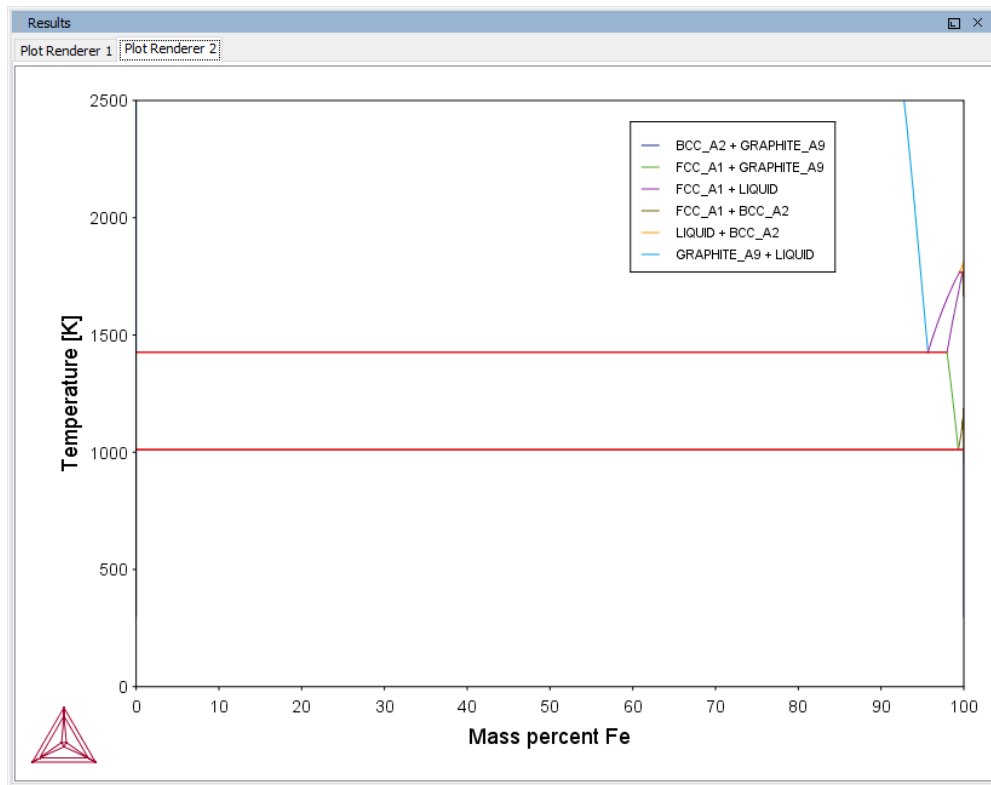
## PLOT RESULTS

### Equilibrium Calculator Results

This shows the plot result of the System Definer and Equilibrium Calculator system.



## Binary Calculator Results



### *T\_04: Fe-Cr-C Ternary Phase Diagram at 1000 K*

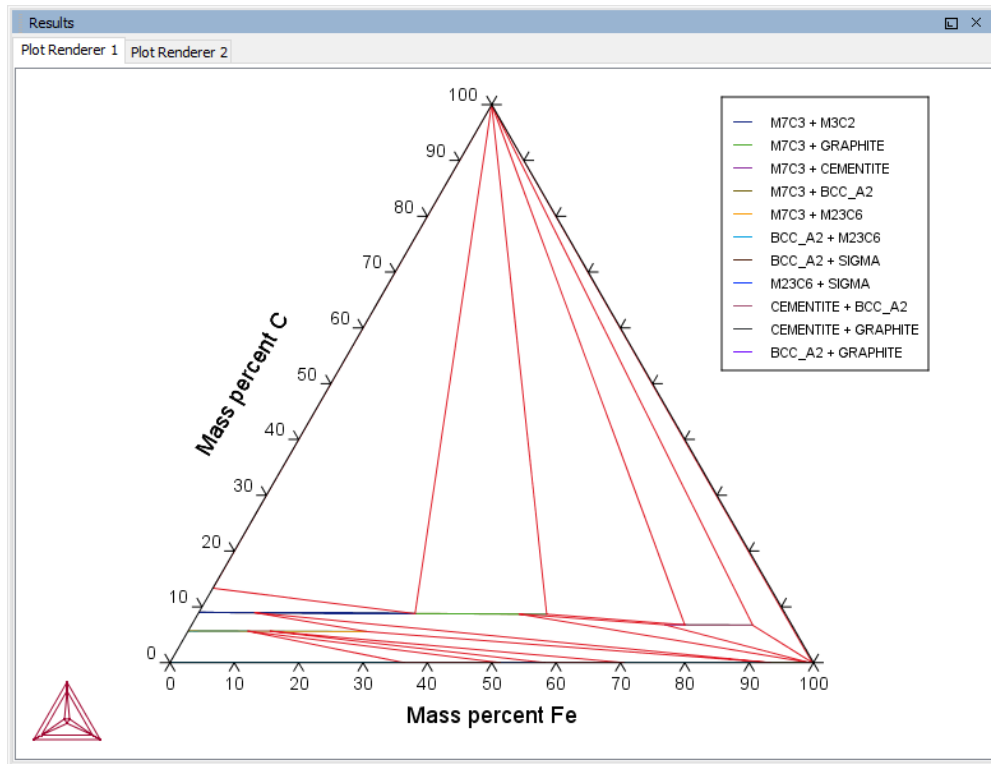
This example shows a ternary phase diagram in the Fe-Cr-C system at 1000 K. Similar to example [T\\_03: Fe-C Phase Diagrams](#), the same diagram is calculated using a Ternary Calculator and then using a System Definer and Equilibrium Calculator. Two Plot Renderer activities are added to create two plots.

## PROJECT FILE AND VIDEO TUTORIAL INFORMATION

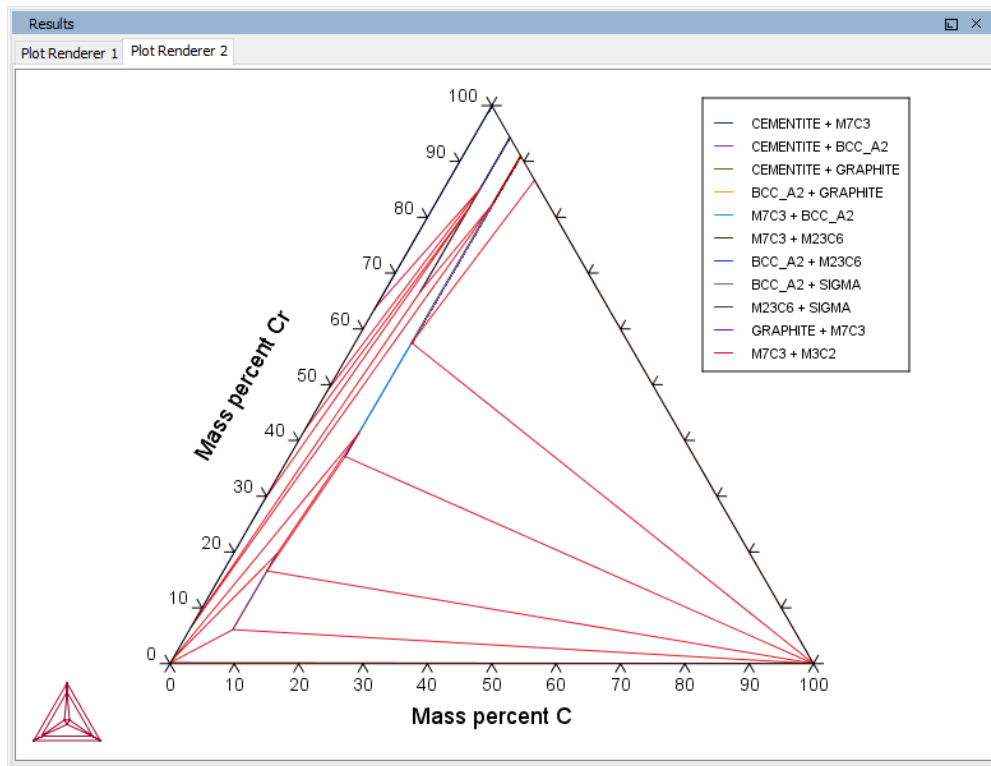
- Folder: Thermo-Calc
- File name: *T\_04\_Fe-Cr-C\_ternary\_phase\_diagram.tcu*
- This example is included in the tutorial on our [website](#) and [YouTube](#) channel.

## PLOT RESULTS

### Ternary Calculator



## Equilibrium Calculator

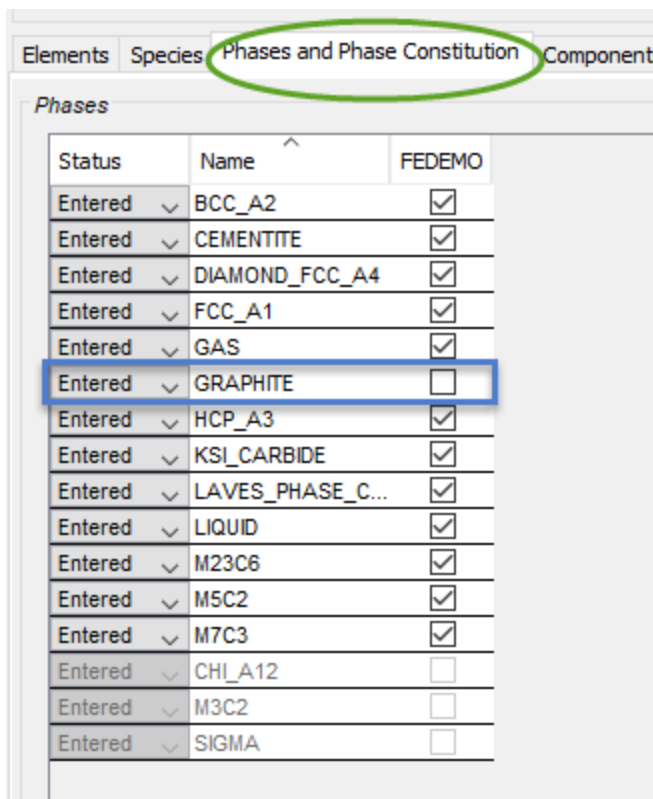


Try practicing with two features on the Plot Renderer Configuration window. To toggle between a triangular and a rectangular diagram, click the **Show Triangular** button then click **Perform** to see what happens. To toggle the X and Y axis variables, click the **Switch Axes** button and then click **Perform**.

### T\_05: Stable and the Metastable Fe-C Phase Diagrams

This example shows how to overlay results from two calculations in the same plot using the Equilibrium Calculator.

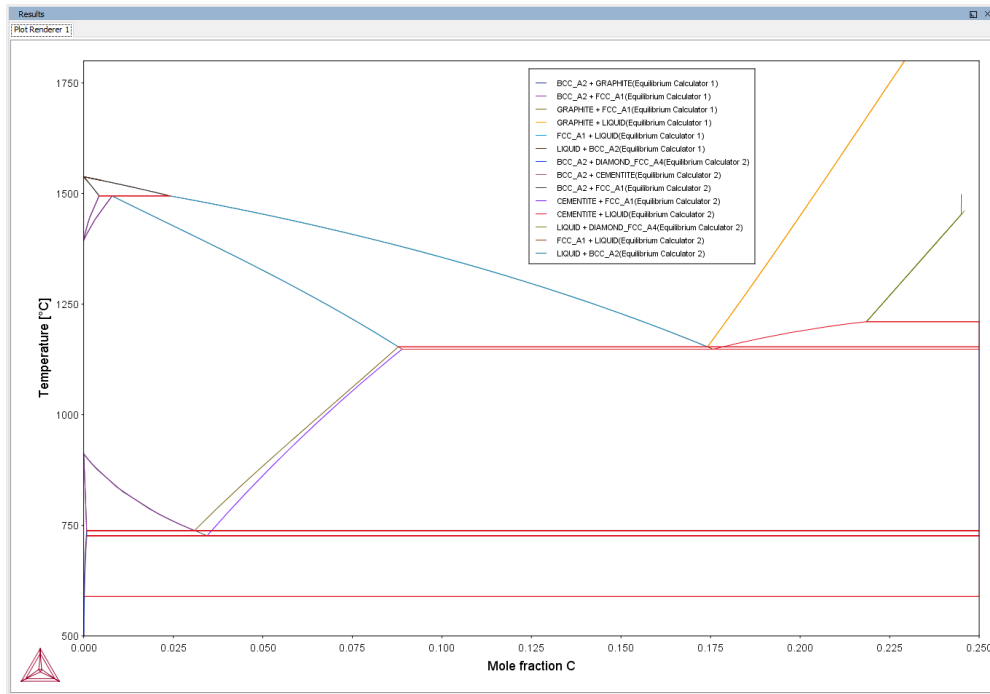
1. The Plot Renderer activity is first created as a successor to Equilibrium Calculator 1.
2. Then right-click the Plot Renderer node and select **Add predecessor** and the results from both equilibrium calculators are in the same plot. In *Equilibrium Calculator 1* the stable phase diagram is calculated and in *Equilibrium Calculator 2* the metastable phase.
3. The metastable diagram is obtained by deselecting the graphite phase on System Definer2 → **Phases and phase constitution** tab.



### PROJECT FILE NAME

- Folder: Thermo-Calc
- File name: T\_05\_Fe-C\_stable\_and\_metastable\_phase\_diagram.tcu

## PLOT RESULT



### *T\_06: Serially Coupled Equilibrium Calculators*

Sometimes there are multiple solutions for a given set of equilibrium conditions. In other cases the equilibrium calculation does not converge. You can then aid the final calculation by, in effect, telling the software where it should start the search for the equilibrium.

This example shows how to serially couple two Equilibrium Calculator nodes together for more complex equilibrium conditions. For each calculation, the output is to a Table Renderer.

## PROJECT FILE NAME

- Folder: Thermo-Calc
- File name: *T\_06\_Serial\_equilibrium\_calculators.tcu*

## Table Renderer Results

### Equilibrium Calculator 1

In the first example, the objective is to calculate the equilibrium at 850° C where the mole fractions of the FCC A1 and BCC A2 phases are 0.5 each for an Fe-Cr-C steel with 10%



chromium. In Equilibrium Calculator 1 a simple set of equilibrium conditions (temperature, pressure, system size and composition) are used to find a carbon content where only the FCC A1 and BCC A2 phases are stable. The results from this preliminary calculation are displayed in Table Renderer 1.

Results				
Table Renderer 1   Table Renderer 2   Table Renderer 3   Table Renderer 4				
<b>System</b>				
Moles	1.00000			
Mass	55.41634	[g]		
Temperature	1123.15000	[K]		
Total Gibbs Energy	-52361.90905	[J]		
Enthalpy	32589.15580	[J]		
Volume	7.34406E-6	[m3]		
<b>Component</b>	<b>Mole Fraction</b>	<b>Mass Fraction</b>	<b>Activity</b>	<b>Potential</b>
C	0.00046	0.00010	0.00137	-61592.91681
Cr	0.10658	0.10000	0.00235	-56531.30746
Fe	0.89296	0.89990	0.00387	-51859.50665
<b>Stable Phases</b>				
<b>BCC_A2#1</b>	<b>Moles</b>	<b>Mass</b>	<b>Volume Fraction</b>	<b>Composition</b>
	0.76777	42.55315	0.76992	
<b>Composition</b>				
<b>Component</b>	<b>Mole Fraction</b>	<b>Mass Fraction</b>		
Fe	0.89183	0.89864		
Cr	0.10801	0.10133		
C	0.00016	0.00003		
<b>FCC_A1#1</b>	<b>Moles</b>	<b>Mass</b>	<b>Volume Fraction</b>	<b>Composition</b>
	0.23223	12.86320	0.23008	
<b>Composition</b>				
<b>Component</b>	<b>Mole Fraction</b>	<b>Mass Fraction</b>		
Fe	0.89669	0.90408		
Cr	0.10185	0.09560		
C	0.00147	0.00032		

## Equilibrium Calculator 2

In Equilibrium Calculator 2 the carbon content equilibrium condition is replaced by the condition that the numbers of moles of the BCC A2 phase should be 0.5. The final result is displayed in Table Renderer 2. In this case, the final objective is to calculate the solidus temperature of an Fe-Cr-C steel with 10% Cr and 0.01% C.

Results				
Table Renderer 1   Table Renderer 2   Table Renderer 3   Table Renderer 4				
<b>System</b>				
Moles	1.00000			
Mass	55.39810	[g]		
Temperature	1123.15000	[K]		
Total Gibbs Energy	-52365.69157	[J]		
Enthalpy	32827.91821	[J]		
Volume	7.32017E-6	[m3]		
<b>Component</b>	<b>Mole Fraction</b>	<b>Mass Fraction</b>	<b>Activity</b>	<b>Potential</b>
C	0.00088	0.00019	0.00146	-60967.89084
Cr	0.10654	0.10000	0.00238	-56409.41447
Fe	0.89258	0.89981	0.00387	-51874.52376
<b>Stable Phases</b>				
	<b>Moles</b>	<b>Mass</b>	<b>Volume Fraction</b>	
<b>BCC_A2#1</b>	0.50000	27.70824	0.50303	Composition ▾
<b>Composition</b>				
<b>Component</b>	<b>Mole Fraction</b>	<b>Mass Fraction</b>		
Fe	0.89000	0.89692		
Cr	0.10982	0.10304		
C	0.00017	0.00004		
	<b>Moles</b>	<b>Mass</b>	<b>Volume Fraction</b>	
<b>FCC_A1#1</b>	0.50000	27.68987	0.49697	Composition ▾
<b>Composition</b>				
<b>Component</b>	<b>Mole Fraction</b>	<b>Mass Fraction</b>		
Fe	0.89515	0.90270		
Cr	0.10326	0.09695		
C	0.00159	0.00034		

### Equilibrium Calculator 3

In Equilibrium Calculator 3 the state at 2000 K is calculated and the result is displayed in Table Renderer 3.

Results				
Table Renderer 1   Table Renderer 2   Table Renderer 3   Table Renderer 4				
<b>System</b>				
Moles	1.00000			
Mass	55.41634	[g]		
Temperature	1123.15000	[K]		
Total Gibbs Energy	-52361.90905	[J]		
Enthalpy	32589.15580	[J]		
Volume	7.34406E-6	[m3]		
<b>Component</b>				
	<i>Mole Fraction</i>	<i>Mass Fraction</i>	<i>Activity</i>	<i>Potential</i>
C	0.00046	0.00010	0.00137	-61592.91681
Cr	0.10658	0.10000	0.00235	-56531.30746
Fe	0.89296	0.89990	0.00387	-51859.50665
<b>Stable Phases</b>				
	<i>Moles</i>	<i>Mass</i>	<i>Volume Fraction</i>	
<b>BCC_A2#1</b>	0.76777	42.55315	0.76992	Composition ▾
<b>Composition</b>				
<i>Component</i>	<i>Mole Fraction</i>	<i>Mass Fraction</i>		
Fe	0.89183	0.89864		
Cr	0.10801	0.10133		
C	0.00016	0.00003		
	<i>Moles</i>	<i>Mass</i>	<i>Volume Fraction</i>	
<b>FCC_A1#1</b>	0.23223	12.86320	0.23008	Composition ▾
<b>Composition</b>				
<i>Component</i>	<i>Mole Fraction</i>	<i>Mass Fraction</i>		
Fe	0.89669	0.90408		
Cr	0.10185	0.09560		
C	0.00147	0.00032		

### Equilibrium Calculator 4

In Equilibrium Calculator 4 the temperature equilibrium condition is replaced by the condition *Fix phase / liquid / 0.0*, meaning that liquid should be stable in an amount of zero moles, i.e. the solidus temperature. The final result is displayed in Table Renderer 4.

Results				
Table Renderer 1   Table Renderer 2   Table Renderer 3   Table Renderer 4				
<b>System</b>				
Moles	1.00000			
Mass	55.41634	[g]		
Temperature	1791.51760	[K]		
Total Gibbs Energy	-1.09463E5	[J]		
Enthalpy	59070.77313	[J]		
Volume	7.63568E-6	[m3]		
<b>Component</b>				
	<i>Mole Fraction</i>	<i>Mass Fraction</i>	<i>Activity</i>	<i>Potential</i>
C	0.00046	0.00010	0.00012	-1.34945E5
Cr	0.10658	0.10000	0.00030	-1.20950E5
Fe	0.89296	0.89990	0.00071	-1.08079E5
<b>Stable Phases</b>				
	<i>Moles</i>	<i>Mass</i>	<i>Volume Fraction</i>	
<b>BCC_A2#1</b>	1.00000	55.41634	1.00000	Composition ▾
<b>Composition</b>				
	<i>Mole Fraction</i>	<i>Mass Fraction</i>		
Fe	0.89296	0.89990		
Cr	0.10658	0.10000		
C	0.00046	0.00010		
<b>Fixed Phases</b>				
	<i>Moles</i>	<i>Mass</i>	<i>Volume Fraction</i>	
<b>LIQUID#1</b>	0.00000	0.00000	0.00000	Composition ▾
<b>Composition</b>				
	<i>Mole Fraction</i>	<i>Mass Fraction</i>		
Fe	0.88607	0.89447		
Cr	0.11178	0.10506		
C	0.00216	0.00047		

### T\_07: User-Defined Functions

This example shows how to implement user-defined functions.

A series of equilibria for an Fe-Cr-C alloy are calculated by varying temperature between 500 and 3000 K. In the configuration window of the Equilibrium Calculator under the **Functions** tab, two identically meaning functions are defined, *fraction solid* and *f solid*, the values of which are plotted against temperature in two Plot Renderer activities. Functions can be entered in terms of *QuantitiesQ1*, *Q2*, *Q3* and so forth, or by using the Thermo-Calc syntax.

### PROJECT FILE INFORMATION

- Folder: Thermo-Calc
- File name: *T\_07\_User\_defined\_functions.tcu*

## PLOT RESULT

*This plot example shows the result of the fraction solid function.*

Equilibrium Calculator 1

Legend option: Axis quantity Legend style: None

---

**X-axis**

Axis variable: Temperature Kelvin

Axis type: Linear

Limits: 1500.0 to 1700.0 step 250.0 ☐ Automatic scaling

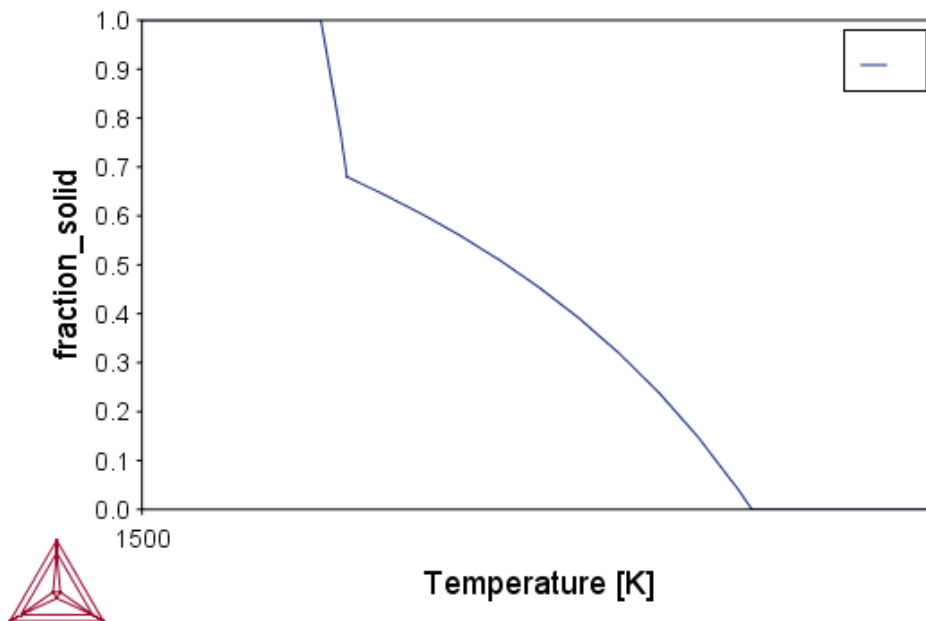
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**Y-axis**

Axis variable: Function fraction\_solid 1-Q1

Axis type: Linear

Limits: 0.0 to 1.0 step 0.1 ☐ Automatic scaling



### ***T\_08: Scheil and Equilibrium Solidification***

This example shows a comparison for an Al-Si alloy solidified under full local equilibrium and under the Scheil assumptions, i.e. zero diffusion in the solidified material and infinitely fast diffusion in the liquid. The example uses the Scheil Calculator and adds a Plot and Table Renderer.

### **PROJECT FILE AND VIDEO TUTORIAL INFORMATION**

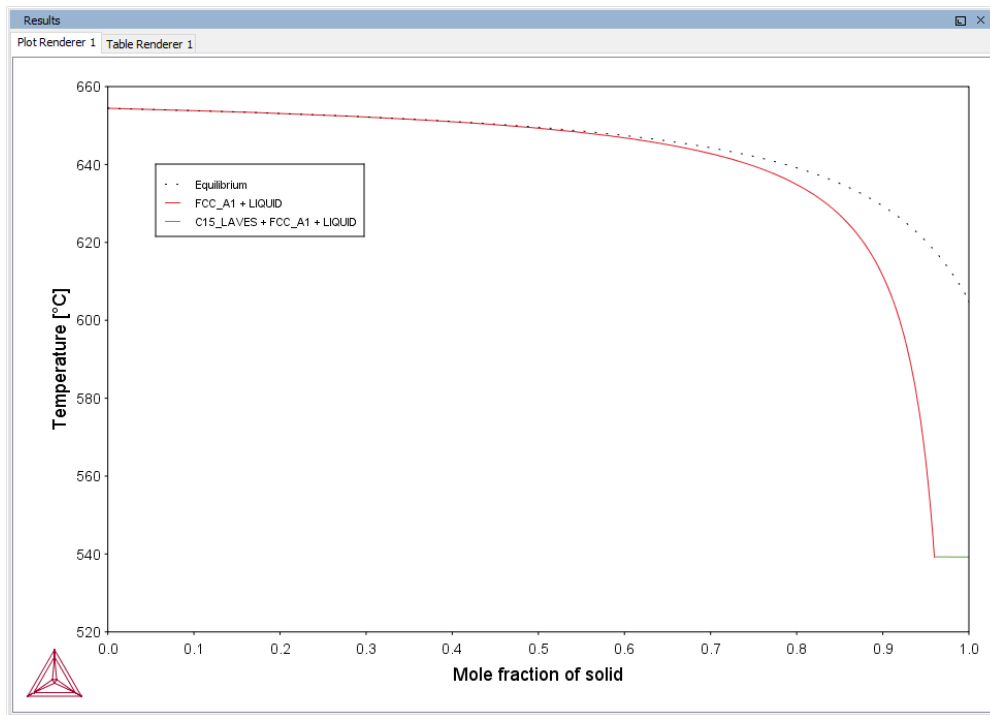
- Folder: Thermo-Calc
- File name: *T\_08\_Scheil\_and\_equilibrium\_solidification.tcu*.

For other examples of using Scheil, see our [website](#) and YouTube channel:

- ▶ [Modified Austenitic Stainless Steel 18/8 Scheil Solidification Simulation](#)
- ▶ [Applications to Welding and Joining with Bonus Scheil Example](#)

## TABLE AND PLOT RESULTS

The plot compares the mole fraction of a solid vs temperature. The table provides the data, which you can also export.



Results

Plot Renderer 1 Table Renderer 1

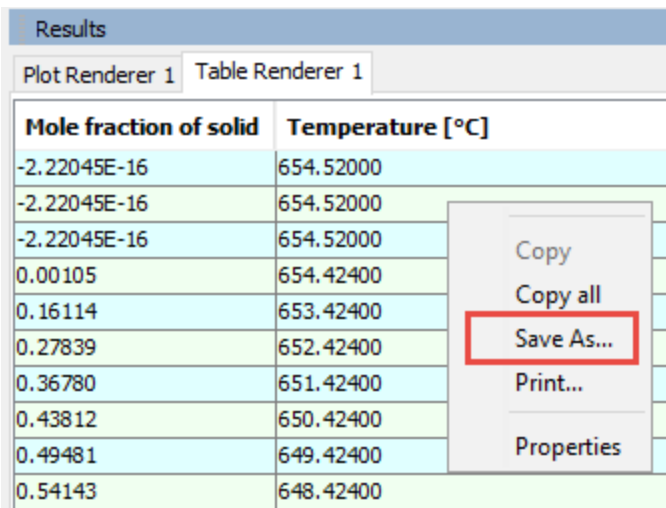
Mole fraction of solid	Temperature [°C]
-2.22045E-16	654.52000
-2.22045E-16	654.52000
-2.22045E-16	654.52000
0.00105	654.42400
0.16114	653.42400
0.27839	652.42400
0.36780	651.42400
0.43812	650.42400
0.49481	649.42400
0.54143	648.42400

## To SAVE THE TABLE

There are two ways to save the table.

### Method 1

In the **Results** window, right click the table and select **Save As...**

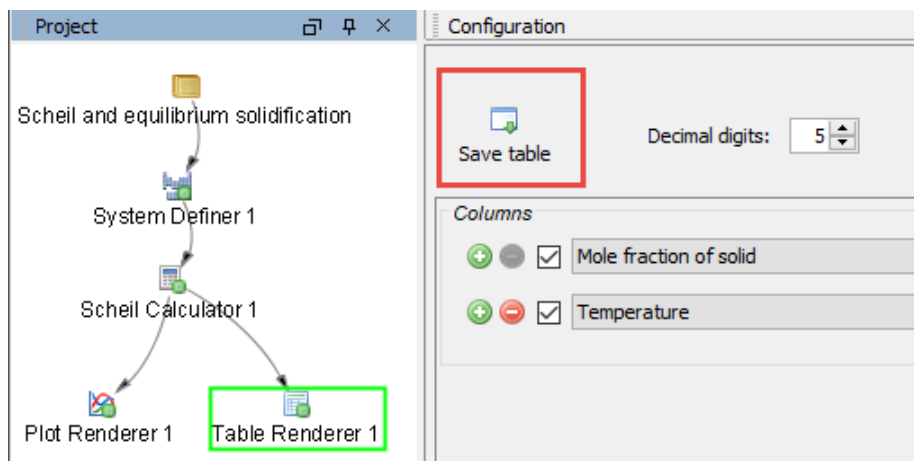


Mole fraction of solid	Temperature [°C]
-2.22045E-16	654.52000
-2.22045E-16	654.52000
-2.22045E-16	654.52000
0.00105	654.42400
0.16114	653.42400
0.27839	652.42400
0.36780	651.42400
0.43812	650.42400
0.49481	649.42400
0.54143	648.42400

Context menu options: Copy, Copy all, **Save As...**, Print..., Properties

### Method 2

1. In the **Project** window, click the **Table Renderer**.
2. In the **Configuration** window, click **Save table**.





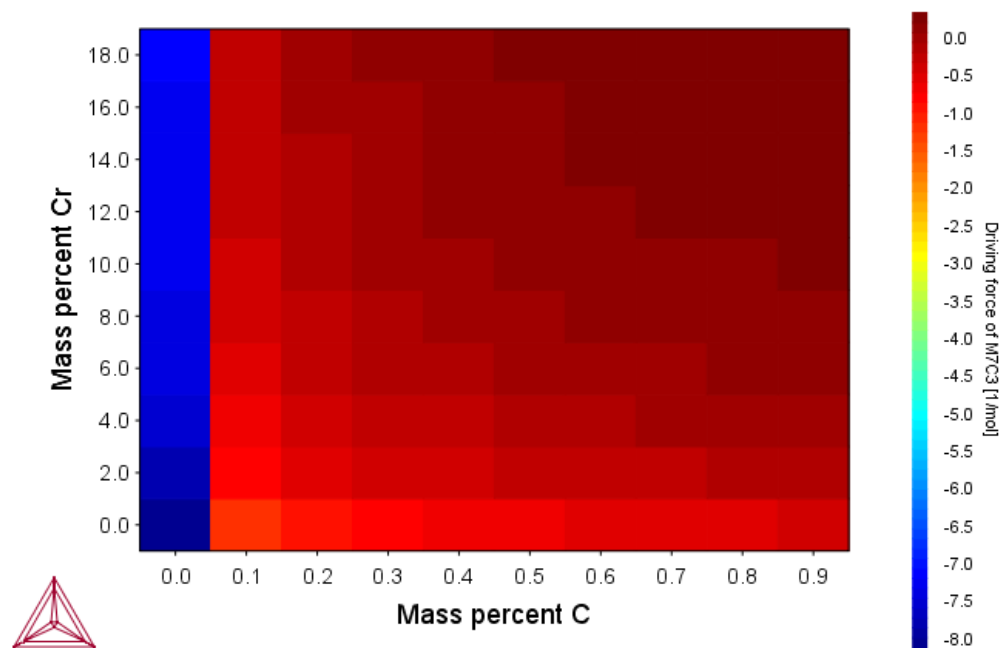
### *T\_09: Carbide Driving Force Heat Map*

This is an example of using *property grid* calculations to plot the driving force for a carbide as a function of two composition variables. With the property grid calculation type, a 2D grid is generated from the two calculation axes. After the calculation is done, an equilibrium is calculated in each grid point. A Plot Renderer connected to a property grid calculator plots the z-axis property for each equilibrium as a function of the two calculation axes. The final plot can be either a heat map or a contour plot.

#### PROJECT FILE NAME

- Folder: Thermo-Calc
- File name: *T\_09\_Heat\_map\_of\_carbide\_driving\_force.tcu*

#### PLOT RESULT



### *T\_10: Phase Transition*

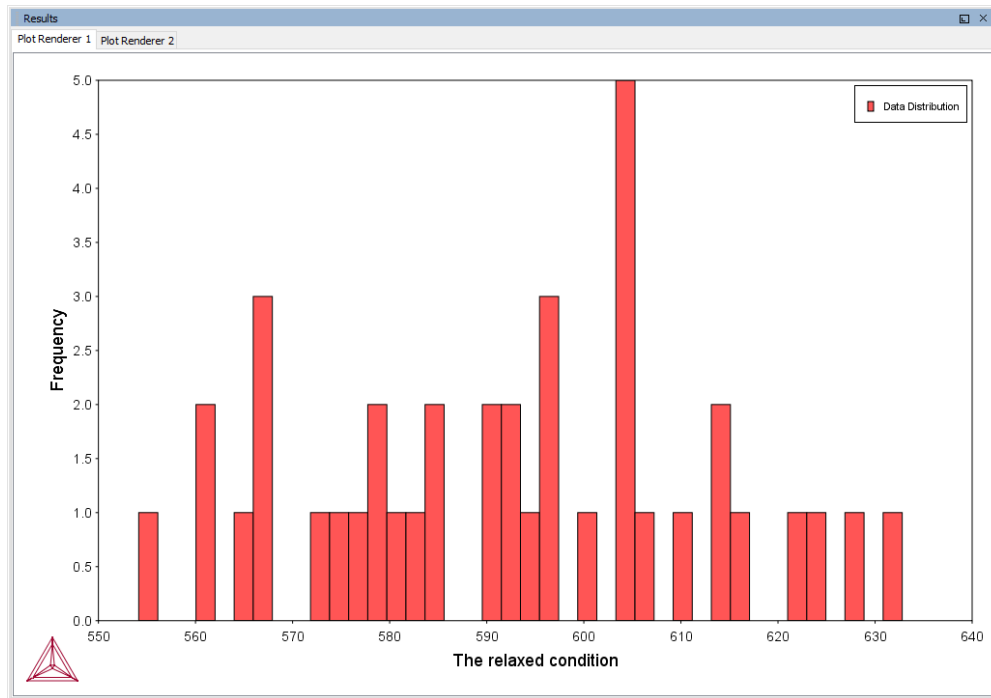
The example uses the Property Model Calculator to predict the transition temperature to the unwanted brittle Sigma phase. The example shows how the temperature is influenced by changes to a steel alloy's composition using the *uncertainty* calculation type and how to create either a *histogram* or *probability* plot.

## PROJECT FILE AND VIDEO TUTORIAL INFORMATION

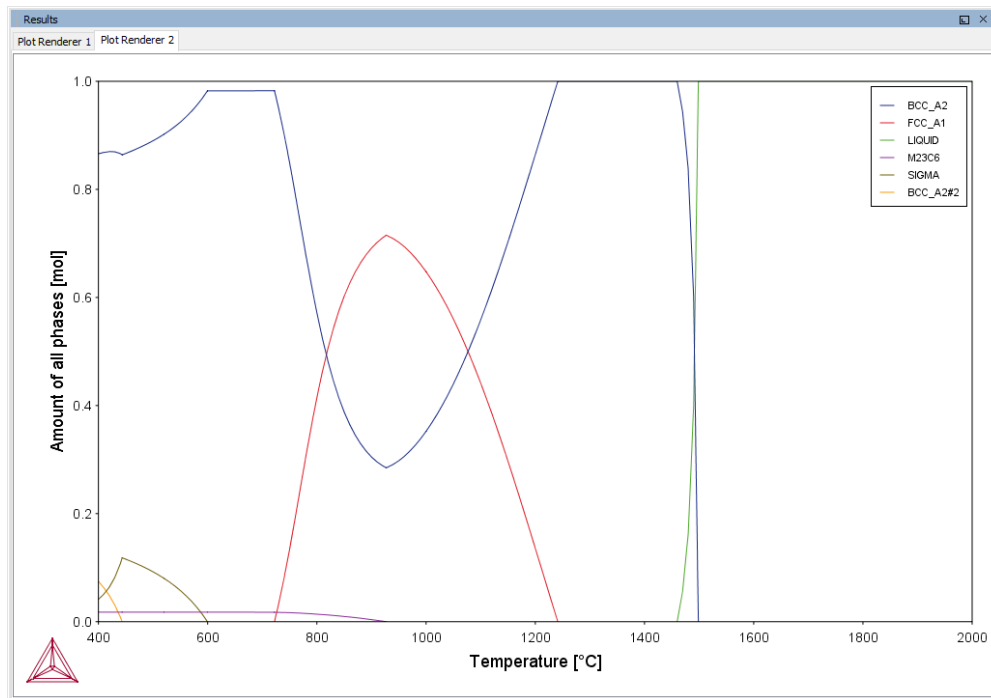
- Folder: Thermo-Calc
- File name: *T\_10\_Phase\_Transition.tcu*
- This example is included in the tutorial on our [website](#) and [YouTube](#) channel. Also see the [video introduction](#) to this feature.

## PLOT RESULTS

### Histogram plot



### Probability plot





Experienced users can also create custom property models for use with the Property Model Calculator.

► Search for Property Model Calculator and Development Framework in the help.

### ***T\_11: Coarsening and Interfacial Energy***

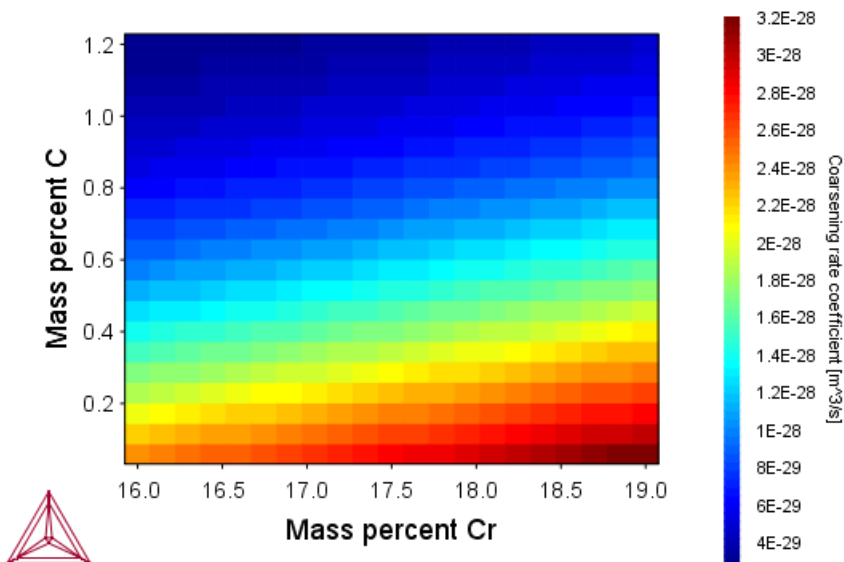
The example uses the Property Model Calculator and both thermodynamic and kinetic demonstration steel databases. Using a *grid* calculation type it produces these plots: a *heat map*, a *contour plot* and a *cross plot with contour* (where both the interfacial energy and coarsening rate is shown). It also creates a property diagram to show the phase fractions vs time and a 3D plot comparing the coarsening rate coefficient.

### **PROJECT FILE AND VIDEO TUTORIAL INFORMATION**

- Folder: Thermo-Calc
- File name: *T\_11\_Coarsening\_and\_Interfacial\_energy.tcu*
- This example is included in the tutorial on our [website](#) and our [YouTube](#) channel. Also see the [video introduction](#) to this feature.

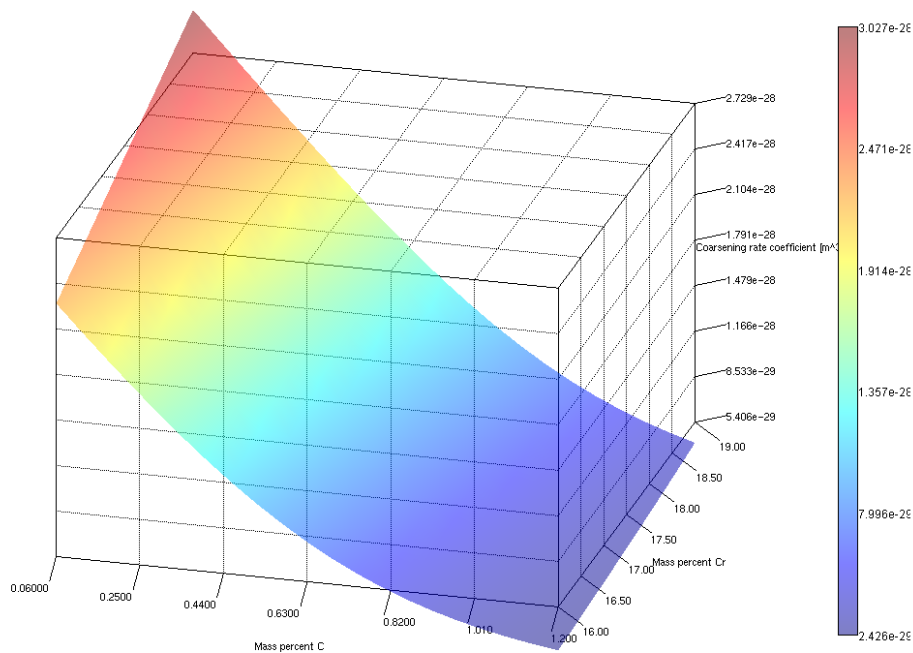
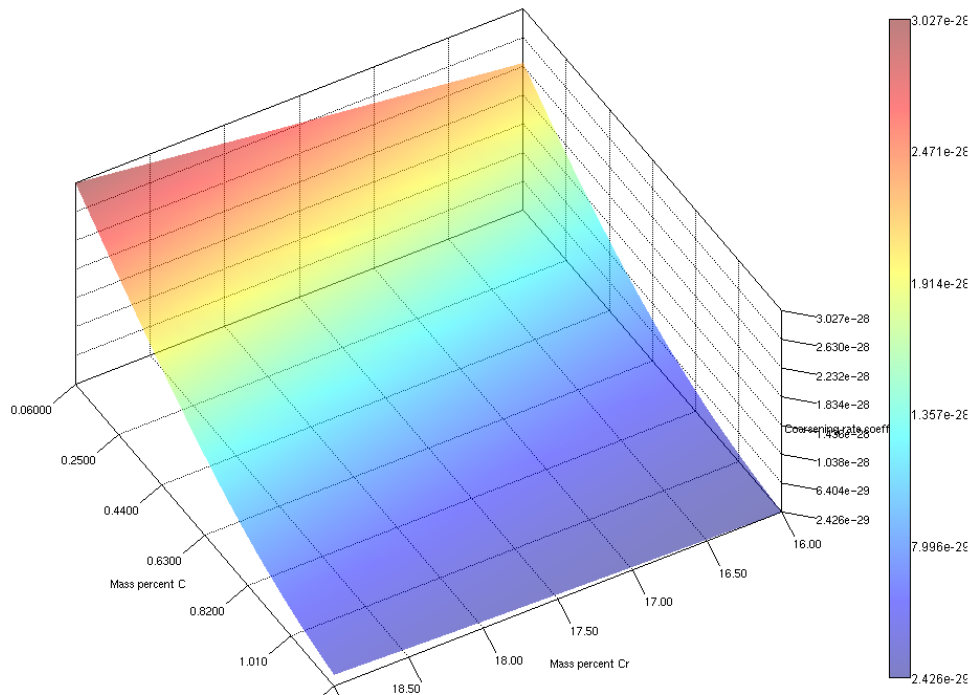
### **Plot Results**

#### **Coarsening rate coefficient (heat map)**



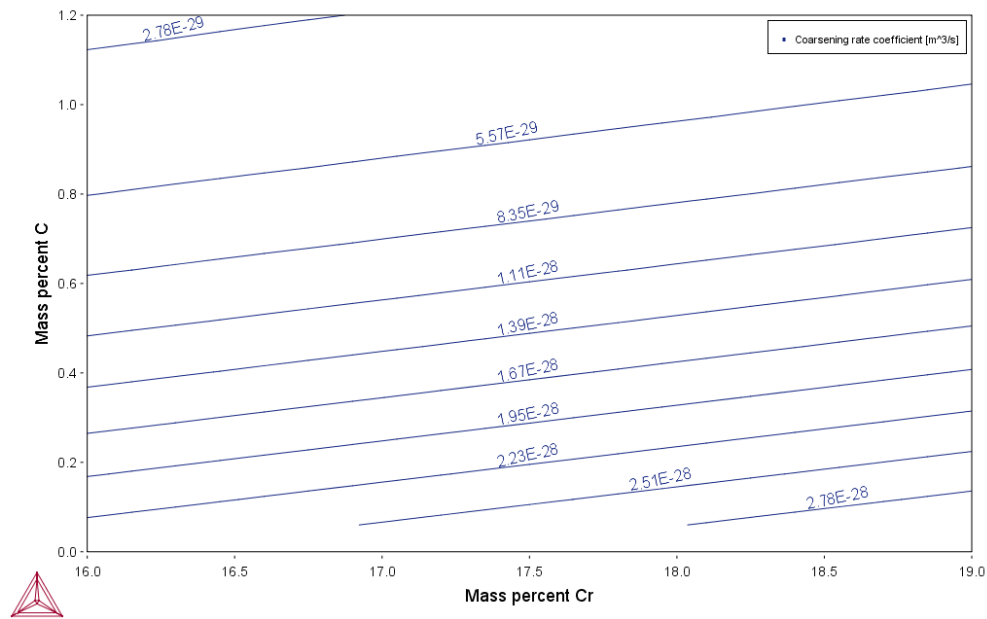
### Coarsening rate coefficient (3D plot)

Two different rotation angles. When viewing in Thermo-Calc you can rotate the plot.

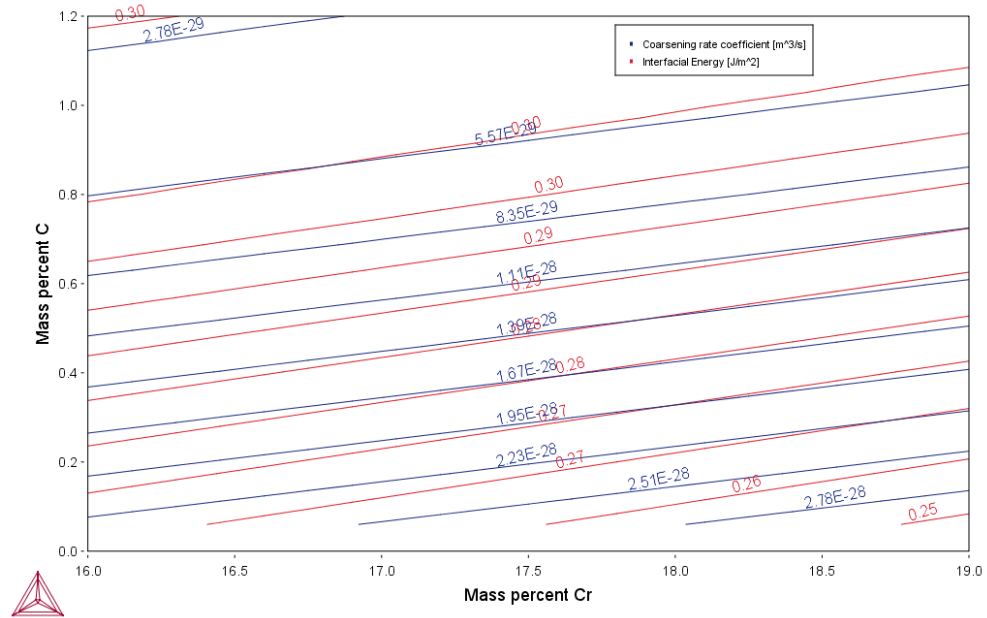


### Coarsening rate coefficient (contour plot)

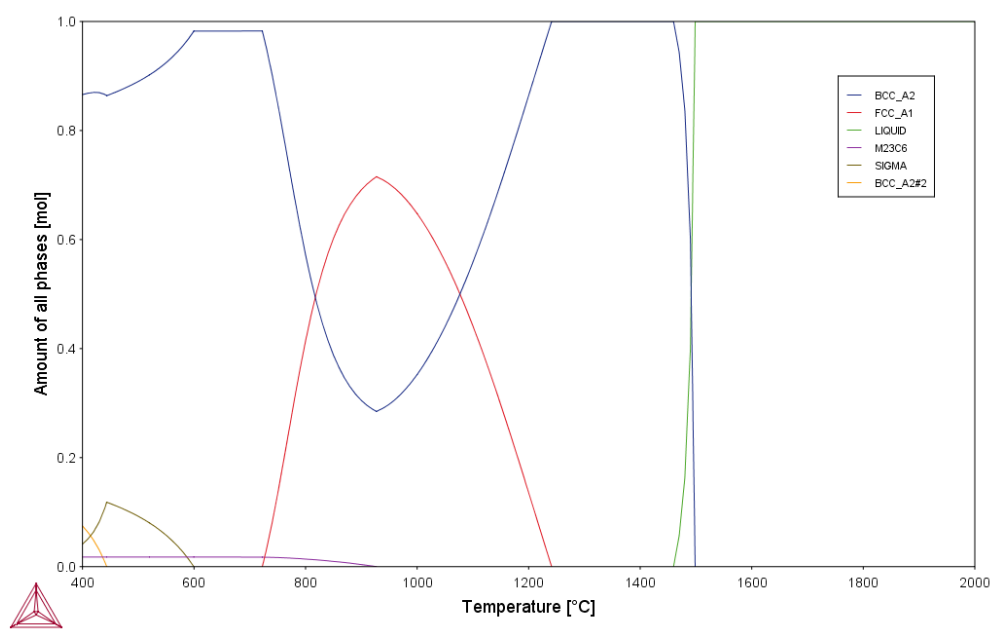
### Coarsening rate coefficient



### Coarsening rate coefficient and Interfacial energy (overlaid plots)



### Phase fractions vs T (Property diagram)



Experienced users can also create custom property models for use with the Property Model Calculator.

► Search for Property Model Calculator and Development Framework in the help.

### ***T\_12: Driving Force and Interfacial Energy***

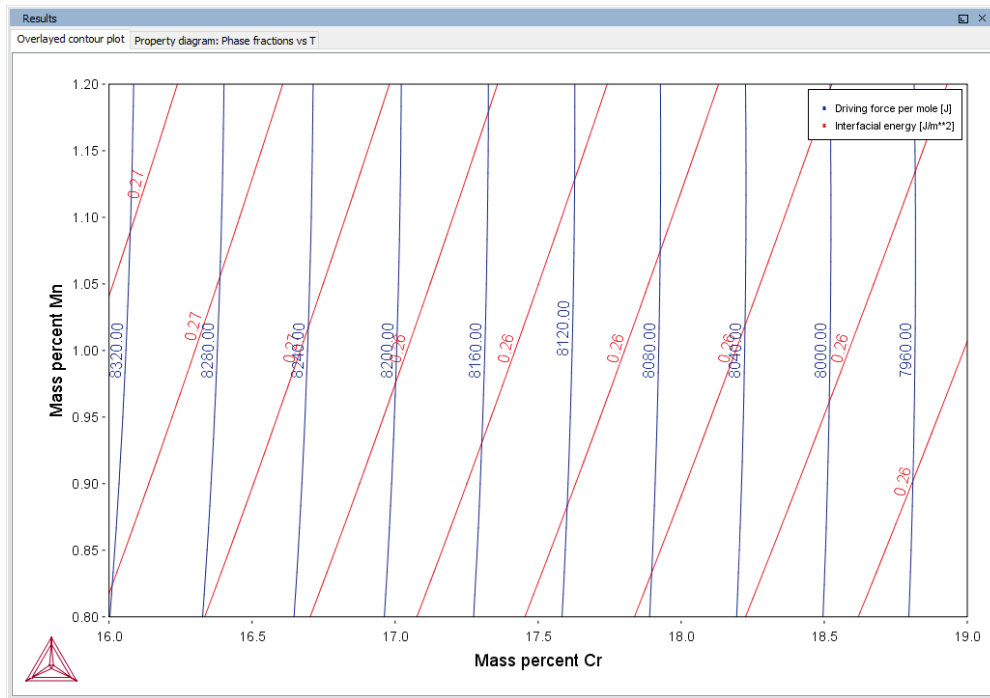
The example uses the Property Model Calculator and a thermodynamic demonstration steel database. Using a *grid* calculation type it produces a *contour* plot comparing the driving force and interfacial energy.

### **PROJECT FILE AND VIDEO TUTORIAL INFORMATION**

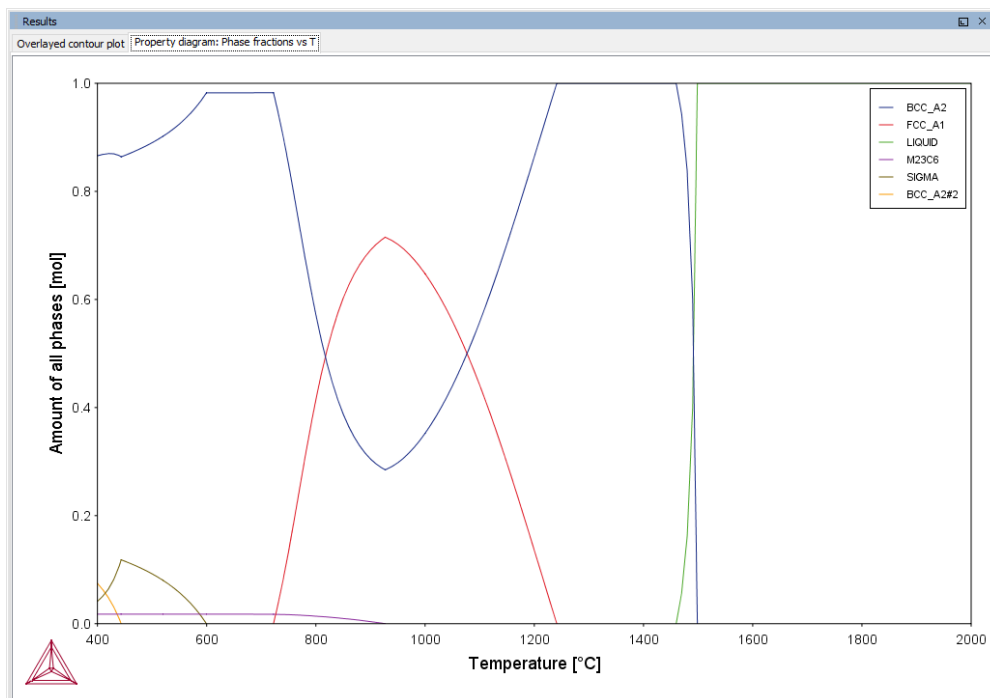
- Folder: Thermo-Calc
- File name: *T\_12\_Driving\_force\_and\_Interfacial\_energy.tcu*
- See the [video introduction](#) to this feature.

## PLOT RESULT

*A contour plot*



*Phase Fraction*







Experienced users can also create custom property models for use with the Property Model Calculator.

▶ Search for Property Model Calculator and Development Framework in the help.

## Diffusion Calculator Examples



Examples using up to three elements are available to all users. The other examples require a Diffusion Module (DICTRA) license to calculate and plot results.



All examples use demonstration database packages included with your installation no matter what licenses you have.

▶ "Diffusion Calculator" in the *Thermo-Calc User Guide*

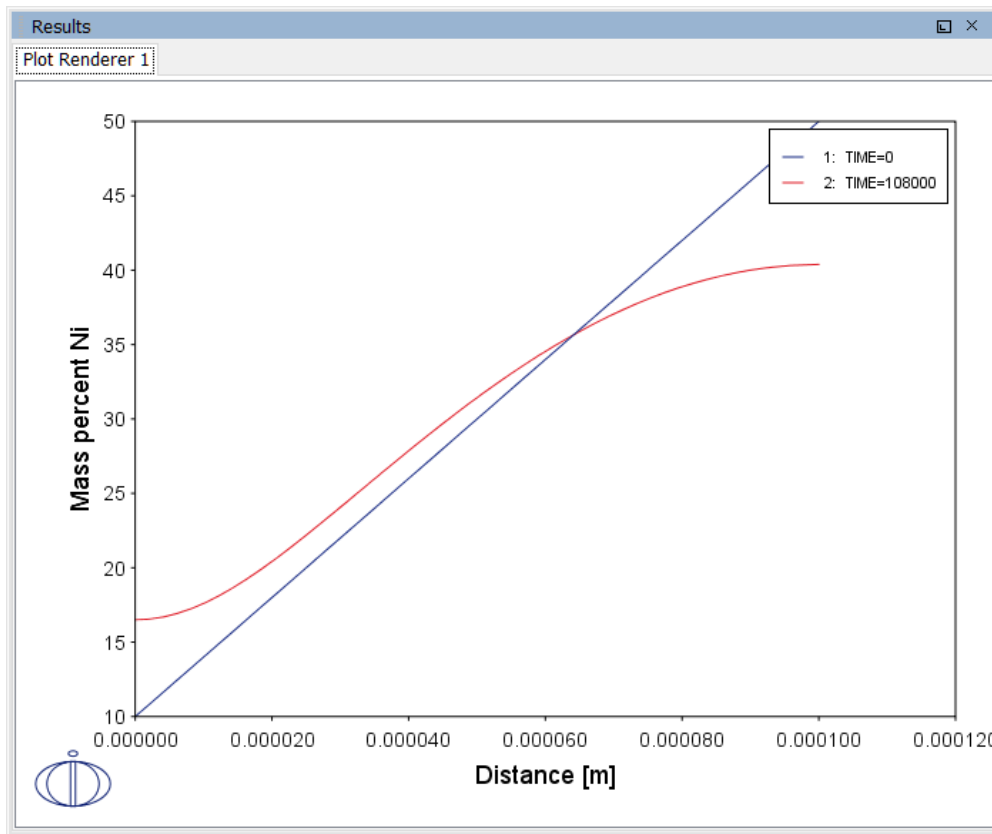
### ***D\_01 Homogenization of a Binary Fe-Ni Alloy***

The single phase example simulates the diffusion of Fe and Ni at a temperature of 1400 K in a planar domain. At this temperature the material is fully austenitic, i.e. the only phase present is the so-called fcc (face centered cubic) phase. Initially, there is a linear variation in Ni going from 10 mass-% on the left-hand side to 50 mass-% on the right-hand side.



This example is available as a video tutorial on [our website](#) and [YouTube channel](#). In previous versions of the software (prior to 2017b) it is example 19.

### Composition of Ni vs Distance



### PROJECT FILE NAME

- Folder: Diffusion Module - DICTRA
- File name: *D\_01\_Diffusion\_Single\_Phase.tcu*



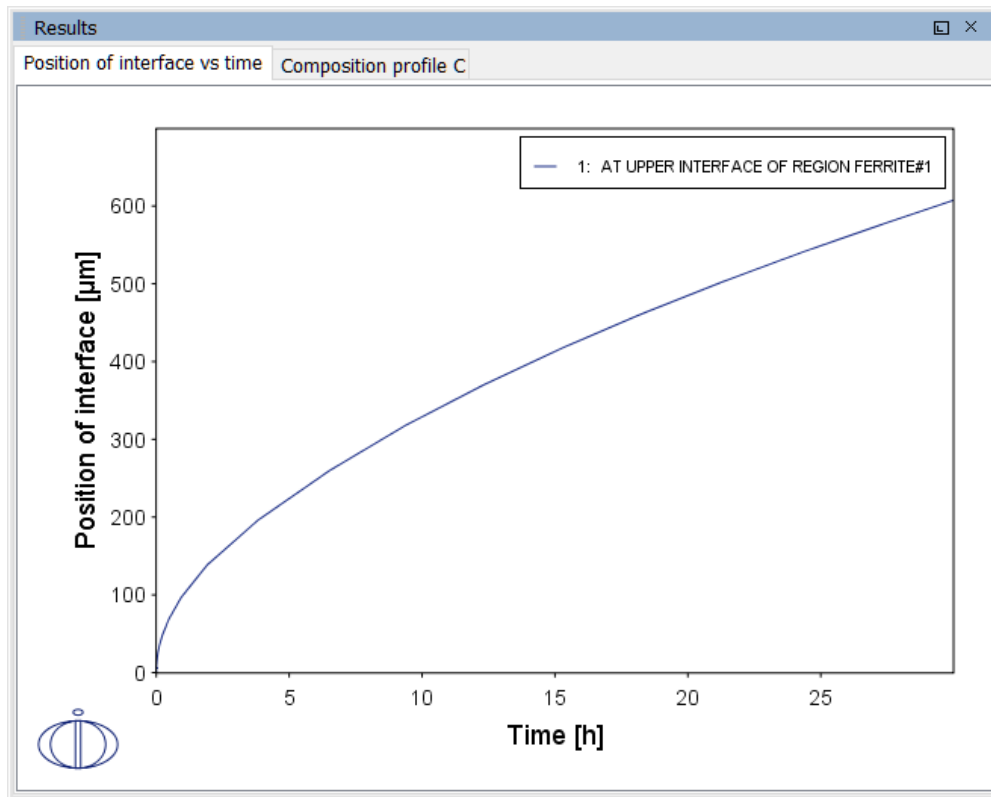
This example is part of the *Diffusion Module (DICTRA) Quick Start Guide* available to all users. A version of the example is also available for Console Mode.

### *D\_02 Ferrite(bcc)/Austenite(fcc) Transformation in a Binary Fe-C Alloy*

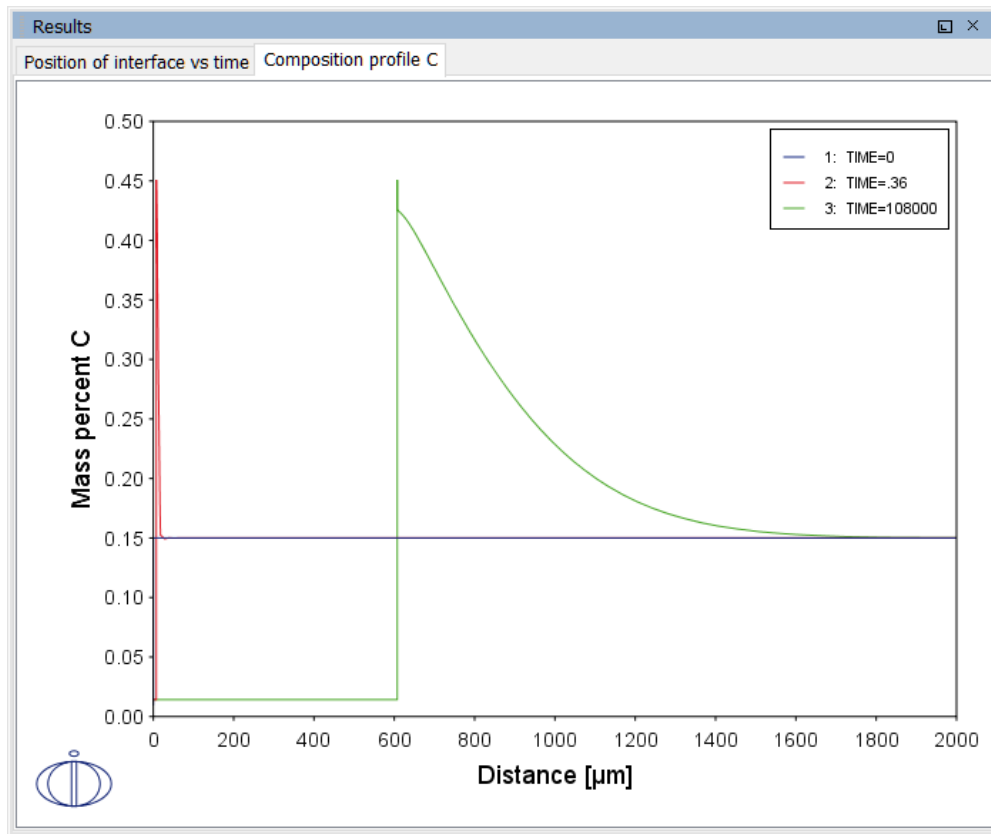
The moving phase boundary example simulates the growth of ferrite (bcc) into austenite (fcc). The austenite is assumed to be initially homogeneous with the composition Fe-0.15 mass-% C. The transformation temperature is 1050 K. The initial thickness of the austenite is 2 mm and an initially very thin ferrite (1 nm) is also present at the start of the simulation.



This example is available as a video tutorial on [our website](#) and [YouTube channel](#). In previous versions of the software (prior to 2017b) it is example 20.

*Position of interface vs time*

### Composition profile C



### PROJECT FILE NAME

- Folder: Diffusion Module - DICTRA
- File name: *D\_02\_Diffusion\_Moving\_Boundary.tcu*



This example is part of the *Diffusion Module (DICTRA) Quick Start Guide* available to all users. A version of the example is also available for Console Mode.

### ***D\_03 Evolution of an Fe-Cr-Ni Diffusion Couple***

The multiphase example simulates the evolution of an Fe-Cr-Ni diffusion couple during a 100 hour heat treatment at 1100° C (1373.15 K). Both end members of the diffusion couple are duplex ferrite plus austenite, but the majority phase is ferrite on the left-hand side and austenite on the right.

With this type of simulation it is assumed that the material is fully equilibrated at each grid point, i.e. the local phase fractions, phase compositions and so forth are obtained from an equilibrium calculation with the local overall composition as a condition.

More details about the homogenization model for multiphase simulations can be found in Larsson and Engström (2006)<sup>1</sup> and Larsson and Höglund (2009)<sup>2</sup>. Experimental data is from Engström (1995)<sup>3</sup>.

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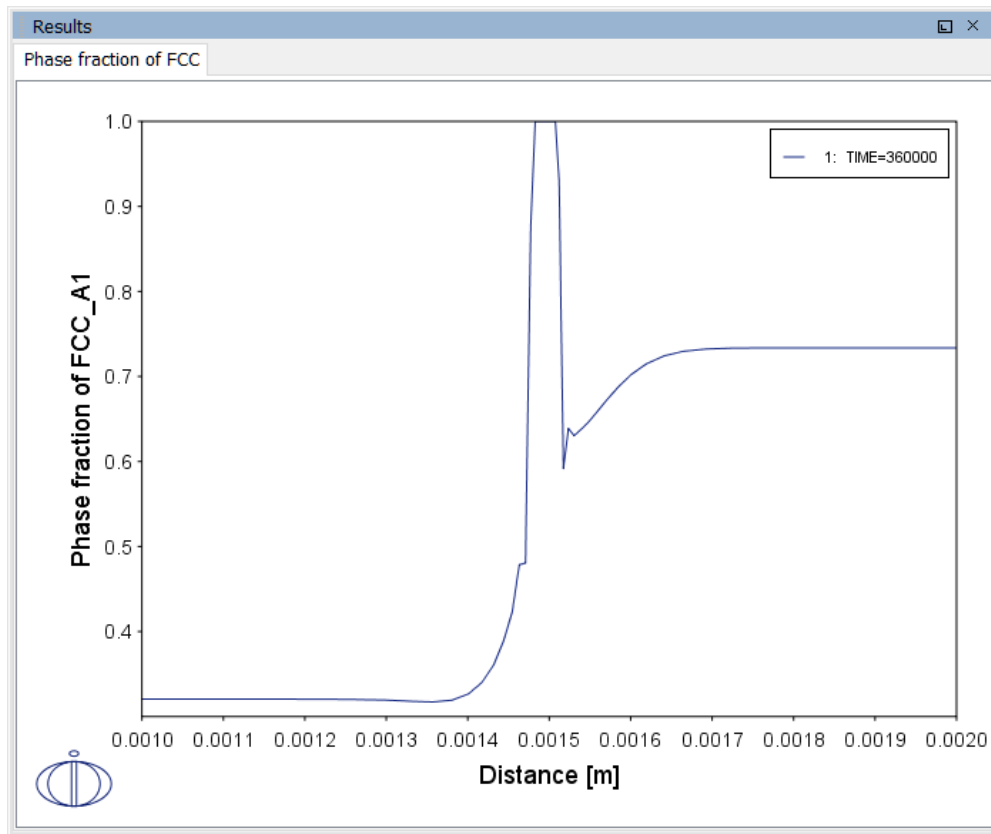
1. "A homogenization approach to diffusion simulations applied to  $\alpha + \gamma$  Fe–Cr–Ni diffusion couples", *Acta Mater.*, 54 (9), pp. 2431–2439.

2. "Multiphase diffusion simulations in 1D using the DICTRA homogenization model", *Calphad*, 33 (3), pp. 495–501.

3. "Interdiffusion in multiphase, Fe-Cr-Ni diffusion couples", *Scand. J. Metall.*, 24(1), 12–20.

---

### Phase fraction of FCC



## PROJECT FILE NAME

- Folder: Diffusion Module - DICTRA
- File name: *D\_03\_Diffusion\_Multiphase.tcu*

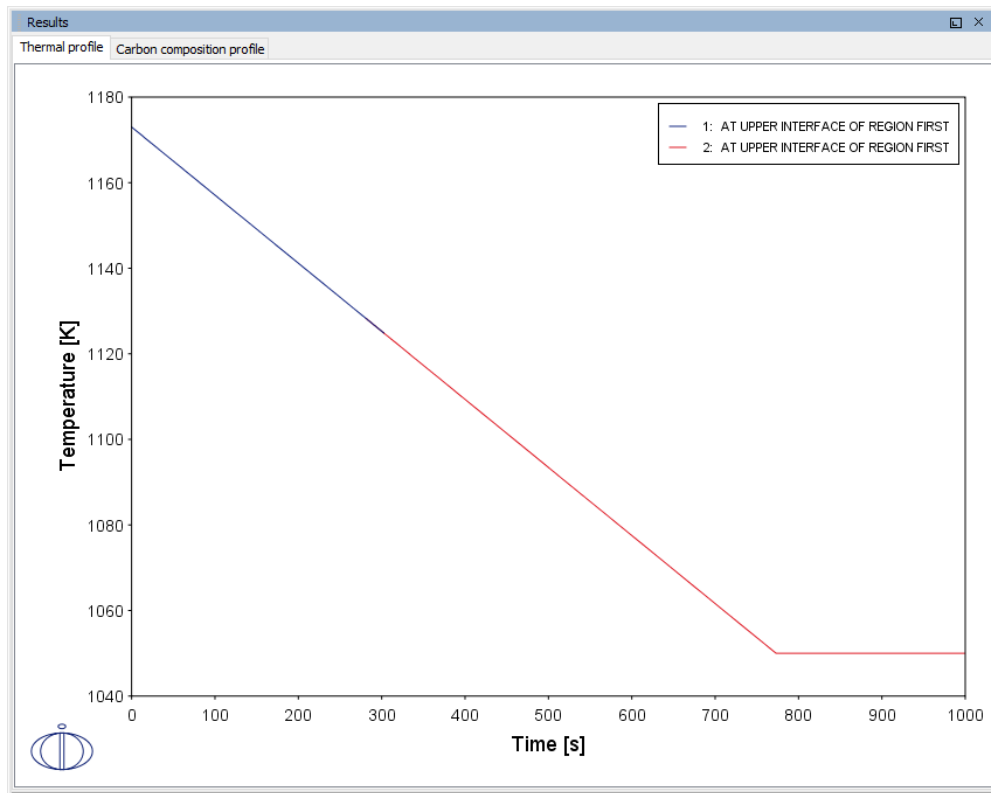


This example is part of the *Diffusion Module (DICTRA) Quick Start Guide* available to all users. A version of the example is also available for Console Mode.

### *D\_04 Fe-C Moving Boundary: Austenite to Ferrite*

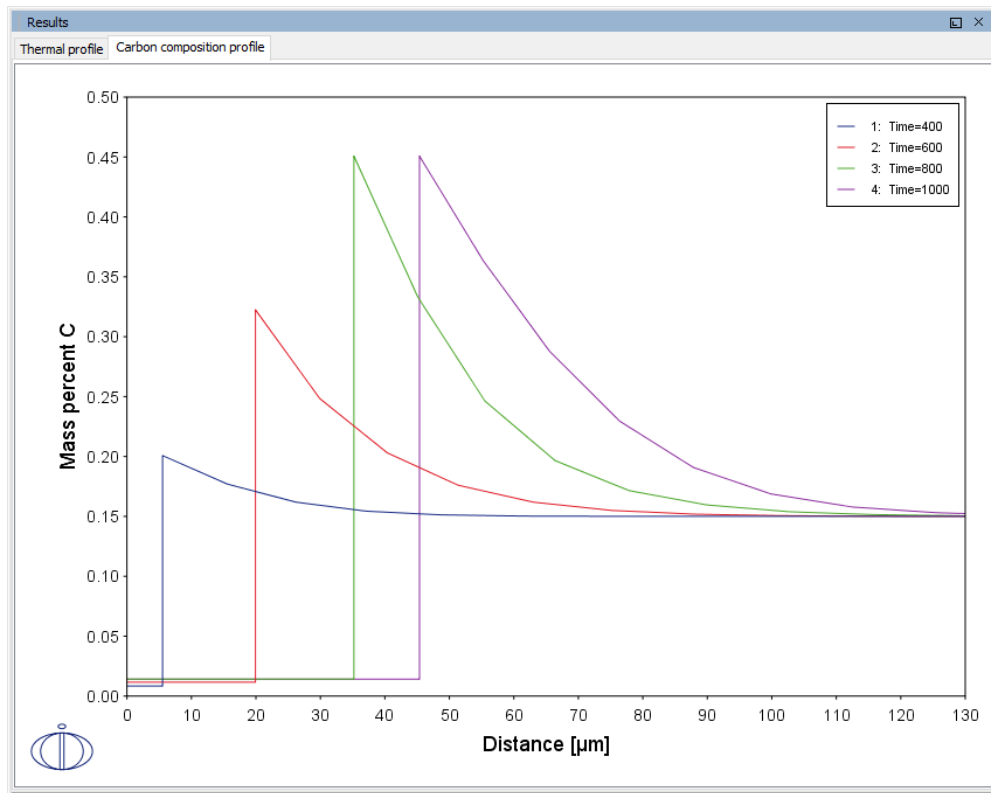
This example simulates the austenite to ferrite transformation in a Fe-0.01 mass% C steel during continuous cooling. The simulation starts at a temperature where only austenite is stable, ferrite nucleates and grows into the austenite during cooling in the two phase region. Plots of thermal and carbon composition profiles are generated.

## Thermal profile





### Carbon composition profile



### PROJECT FILE NAME

- Folder: Diffusion Module - DICTRA
- File name: *D\_04\_Diffusion\_Fe-C\_Moving\_Boundary\_Austenite\_to\_Ferrite.tcu*

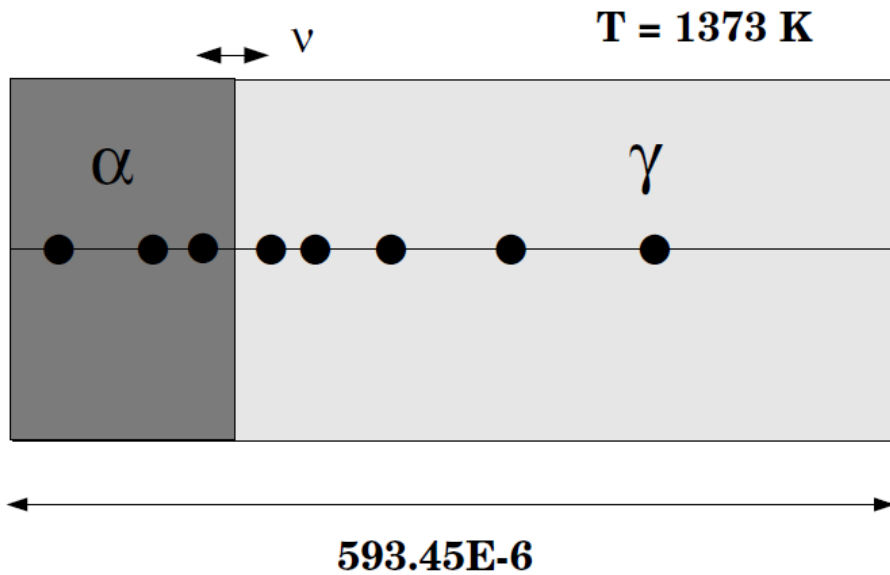


This example is available to all users.

### D\_05 $\gamma/\alpha/\gamma$ Diffusion couple of Fe-Ni-Cr alloys

This example demonstrates the evolution of a ternary Fe-Cr-Ni diffusion couple. A thin slice of ferrite ( $\alpha$  phase) (38%Cr,0%Ni) is clamped between two thicker slices of austenite ( $\gamma$  phase) (27%Cr, 20%Ni). The assembly is subsequently heat treated at 1373 K.

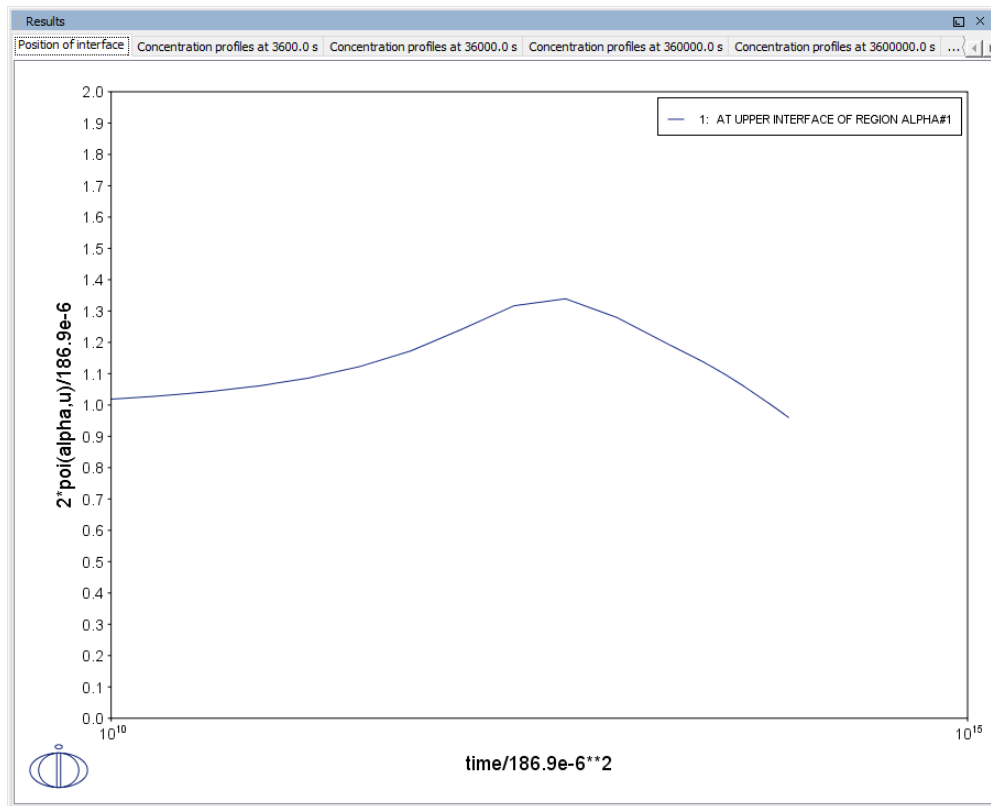
This set up corresponds to diffusion couple in Kajihara, Lim, and Kikuchi (1993)<sup>1</sup>. Also see Kajihara and Kikuchi (1993)<sup>2</sup>.



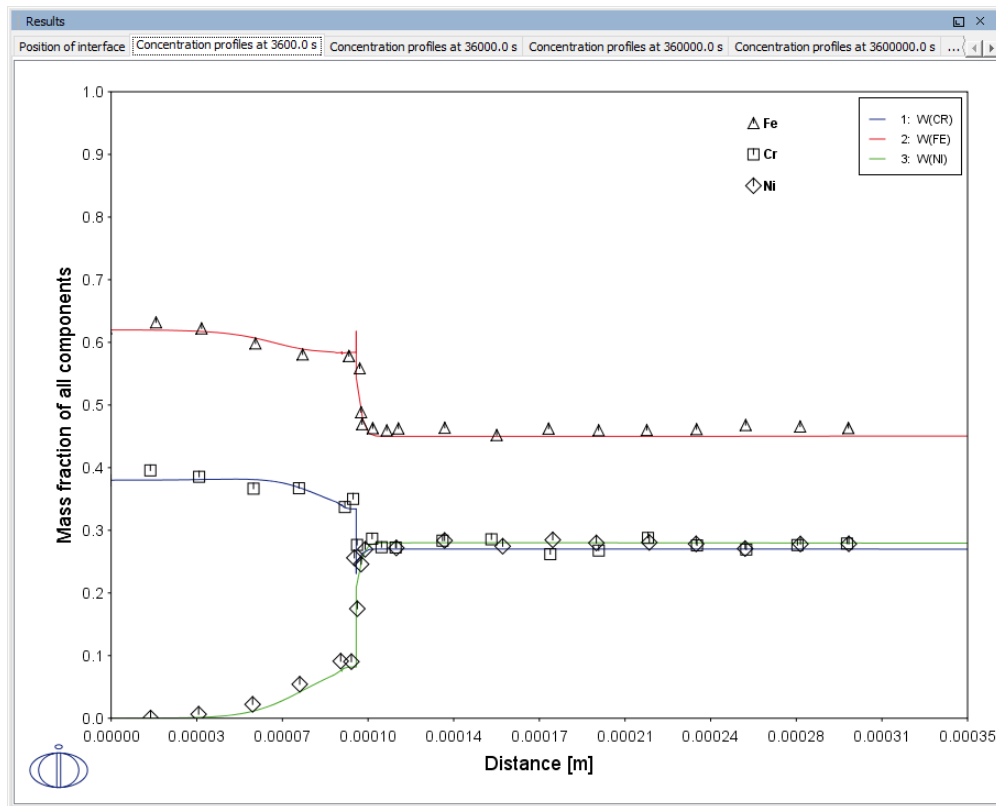
<sup>1</sup>. "Experimental Study on Dissolution of ALPHA Phase in GAMMA/ALPHA/GAMMA Diffusion Couples of the Fe-Cr-Ni System", *ISIJ Int.*, 33(4), 498–507.

<sup>2</sup>. "Numerical analysis of dissolution of  $\alpha$  phase in  $\gamma/\alpha/\gamma$  diffusion couples of the Fe-Cr-Ni system", *Acta Metall. Mat.*, 41(7), 2045–2059.

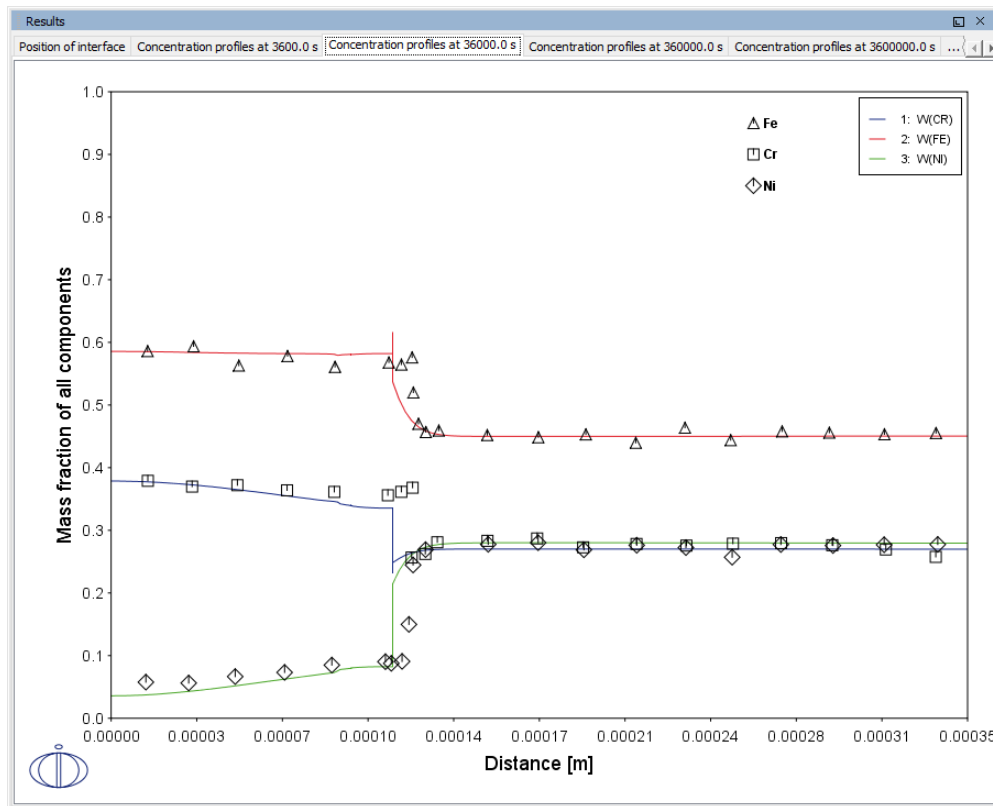
## Interface Position



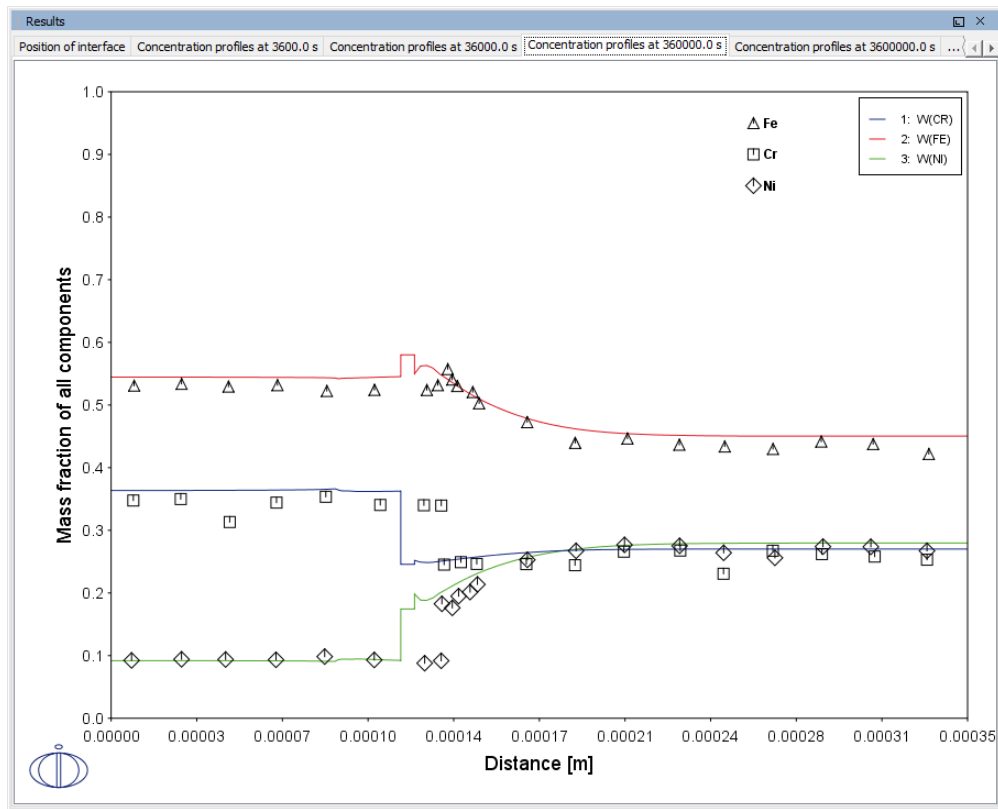
## Concentration profiles at 3600 s



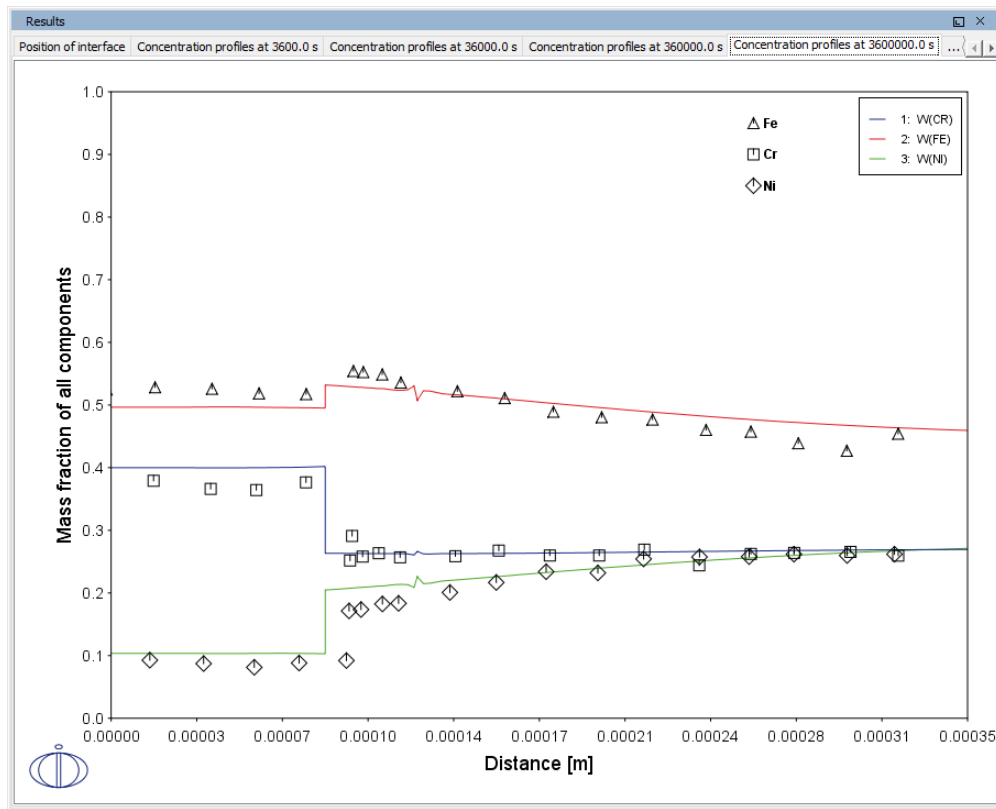
## Concentration profiles at 36000 s



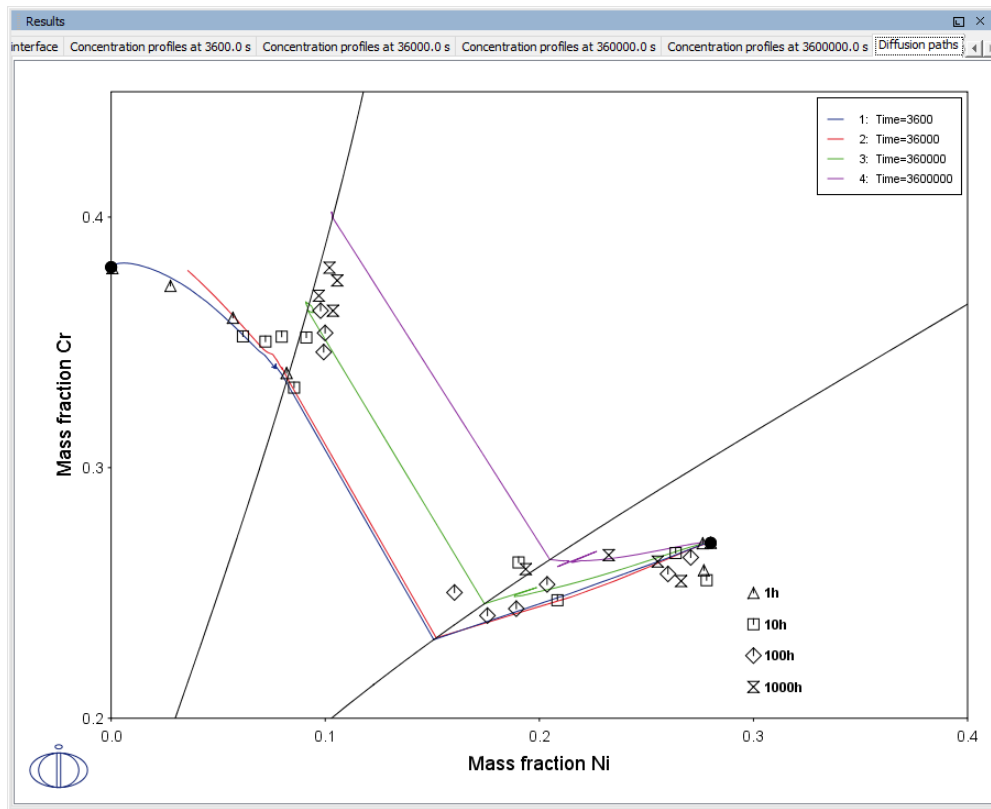
## Concentration profiles at 36 0000 s



## Concentration profiles at 3 600 000 s



## Diffusion paths



## PROJECT FILE NAME

- Folder: Diffusion Module - DICTRA
- File name: *D\_05\_Diffusion\_Fe\_Ni\_Cr\_Moving\_Boundary\_Diffusion\_Couple.tcu*

## D\_06 Diffusion Through a Tube Wall

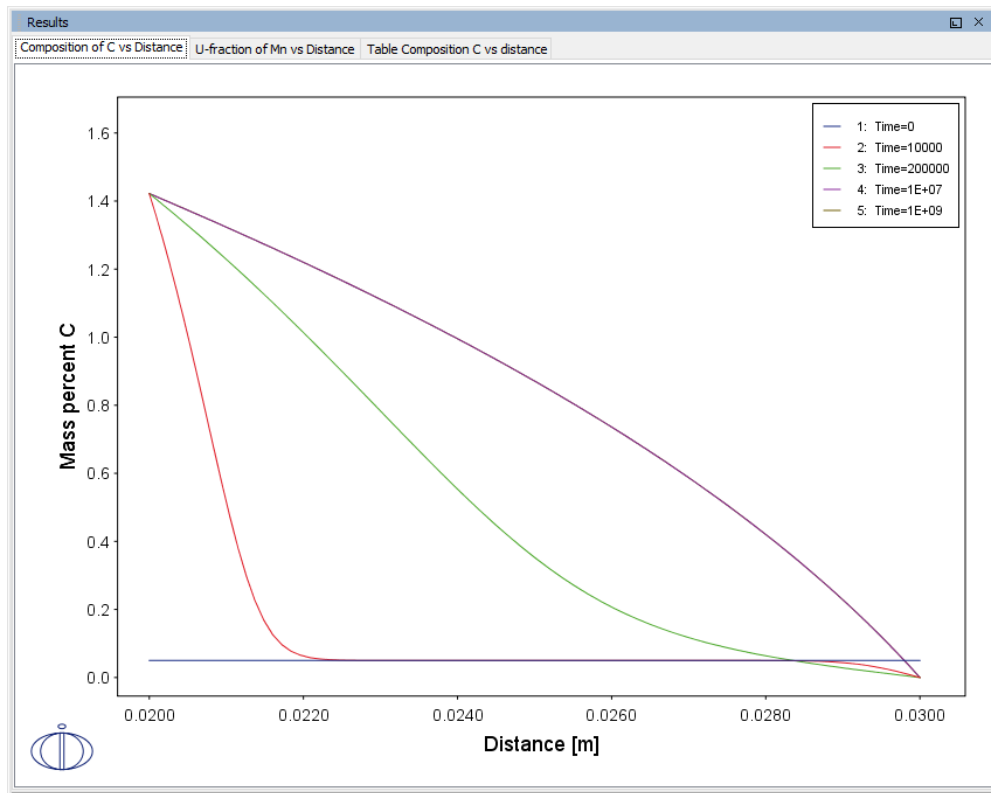
This is a simple example of diffusion through a tube wall. The tube material is an Fe-0.06Mn-0.05C alloy. Two plots comparing distance to the U-fraction of manganese and composition of carbon are generated to visualize the austenite region. A *cylindrical* geometry is used with *mixed zero flux and activity* boundary conditions.

On the inside wall a carbon activity of 0.9 is maintained whereas on the outside the carbon activity is very low. This example demonstrates the use of boundary conditions, advanced plotting and tables.

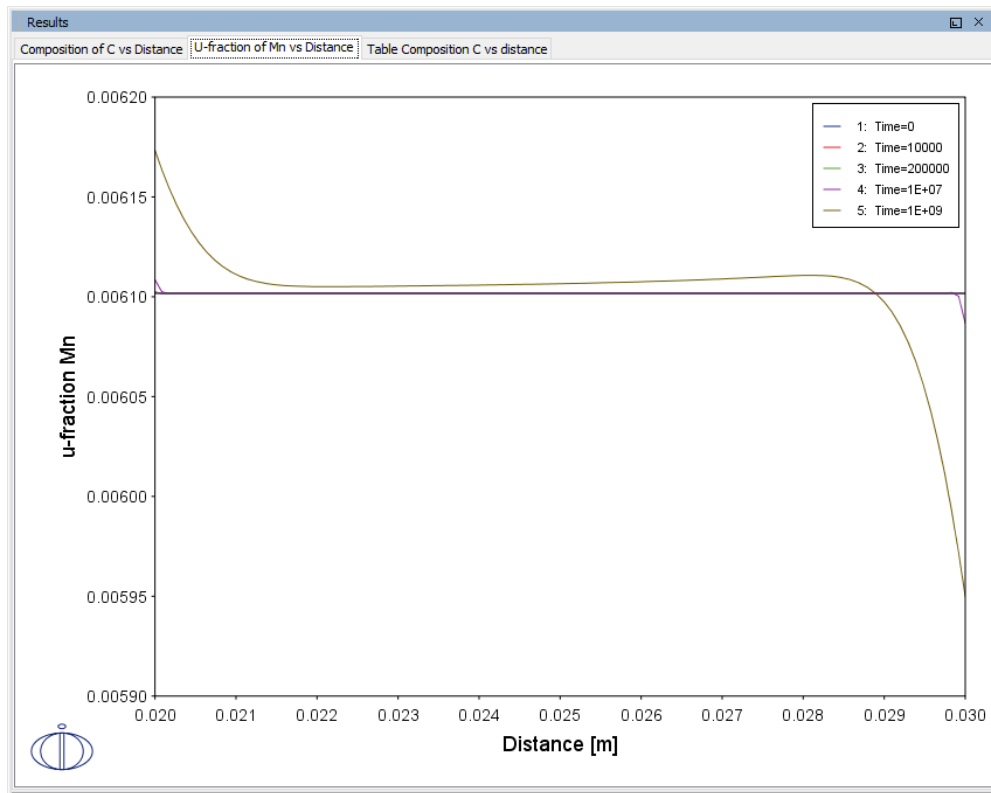


This example is based on Console Mode exab6 (see in the *Diffusion Module (DICTRA) Console Mode Examples Guide*). When in Console Mode, you can open the example from Thermo-Calc (**File** → **Examples Files** → **Diffusion Module**).

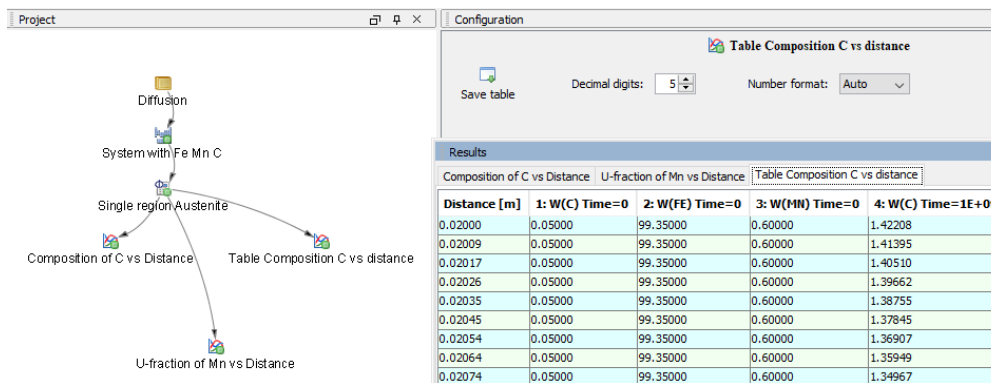


*Composition of C vs Distance*

### U-fraction of Mn vs Distance



### Table Composition C vs Distance



### PROJECT FILE NAME

- Folder: Diffusion Module - DICTRA
- File name: *D\_06\_Diffusion\_Carburization\_Tube.tcu*

### D\_07 Multiphase Carburization of a Ni-25Cr-0.0001C alloy

This example is about carburization of a Ni-25Cr-0.0001C alloy. In this case the M7C3 and M3C2 carbides are entered as spheroid phases in an FCC\_A1 matrix. It is similar to Graphical Mode example D\_06 except the default **Simulation condition** is automatically set to use the **Homogenization** model.

The Isothermal calculation is run for 1000 hours at a temperature of 1123 K using the **Mixed zero flux and activity** left boundary condition. Results are plotted using two Plot Renderers and a Table Renderer.

This case is from Engström, Höglund, and Ågren (1994), "Computer simulation of diffusion in multiphase systems", *Met. Mat. Trans. A*, 25(6), 1127–1134.



This example is based on Console Mode exd1b (see in the *Diffusion Module (DICTRA) Console Mode Examples Guide*). When in Console Mode, you can open the example from Thermo-Calc (**File** → **Examples Files** → **Diffusion Module**).

#### Phase fraction vs distance

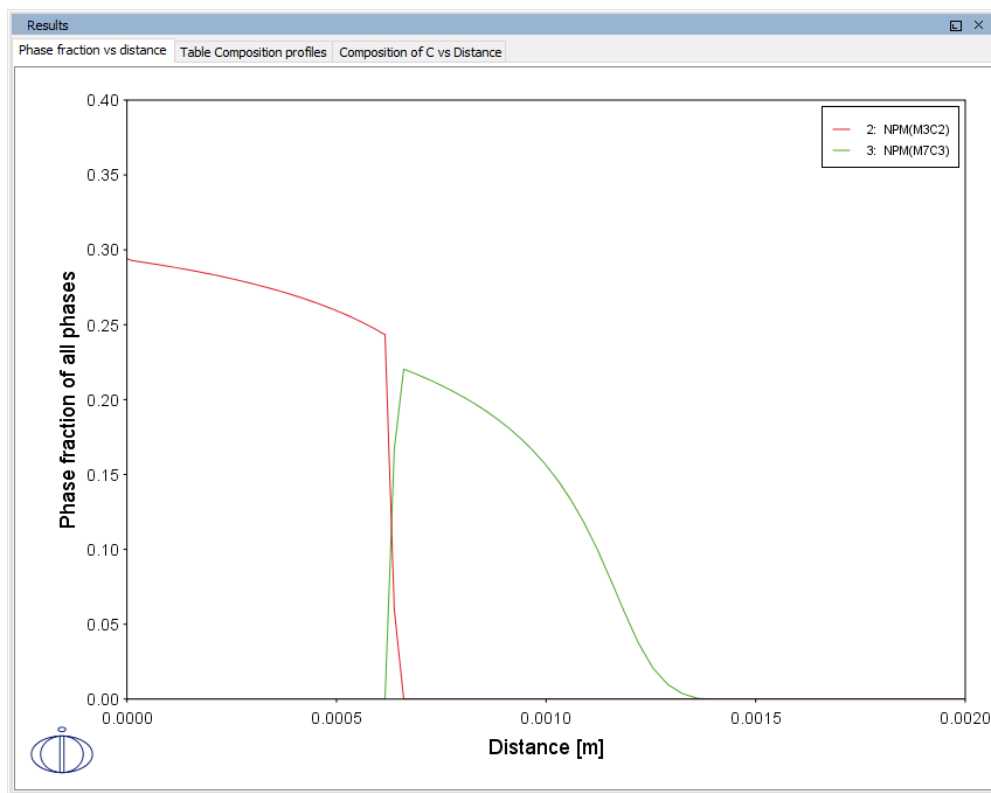
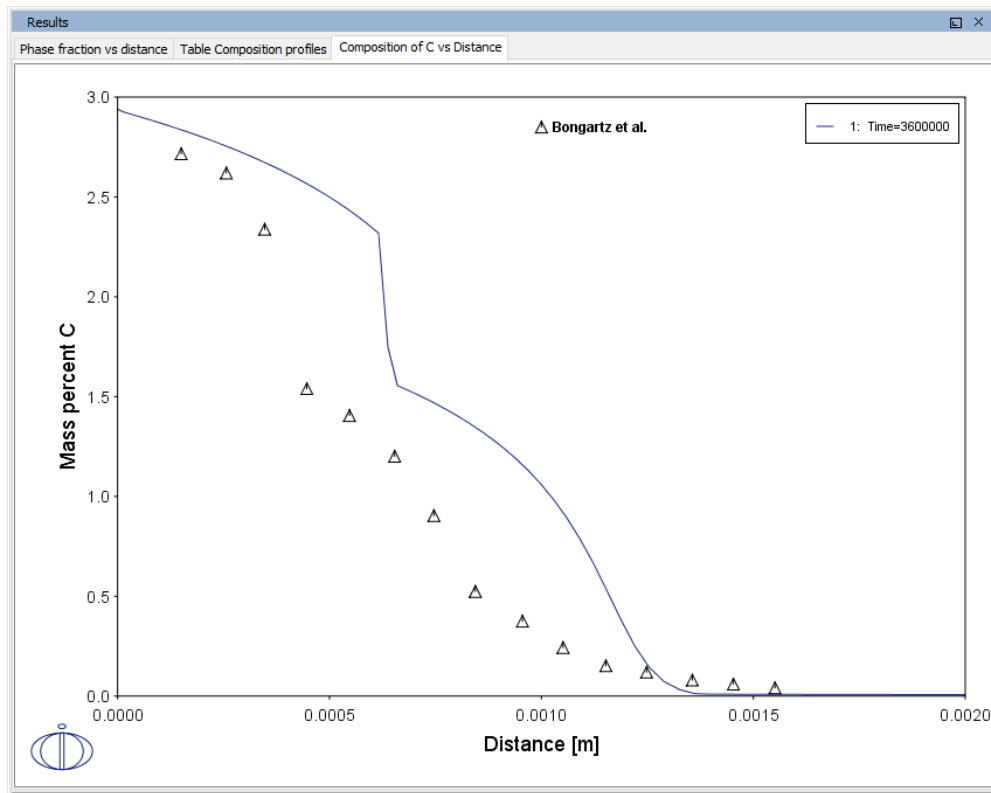


Table of Composition profiles

Results			
Phase fraction vs distance		Table Composition profiles	
		Composition of C vs Distance	
Distance [m]	1: W(C)	2: W(CR)	3: W(HI)
0.00000	2.93966	24.35835	72.70199
9.88104E-6	2.92919	24.27458	72.79623
0.00002	2.92153	24.27324	72.80522
0.00003	2.91543	24.27447	72.81011
0.00004	2.90899	24.27584	72.81517
0.00005	2.90235	24.27733	72.82032
0.00006	2.89549	24.27886	72.82565
0.00007	2.88841	24.28053	72.83106
0.00008	2.88107	24.28222	72.83670
0.00010	2.87349	24.28403	72.84248
0.00011	2.86564	24.28588	72.84849
0.00012	2.85750	24.28783	72.85467
0.00013	2.84907	24.28984	72.86110
0.00014	2.84033	24.29194	72.86773
0.00016	2.83124	24.29412	72.87464
0.00017	2.82181	24.29640	72.88179
0.00018	2.81201	24.29877	72.88922
0.00020	2.80183	24.30124	72.89693
0.00021	2.79122	24.30381	72.90497
0.00022	2.78018	24.30650	72.91332
0.00024	2.76867	24.30930	72.92203
0.00025	2.75666	24.31222	72.93112
0.00027	2.74412	24.31528	72.94060
0.00028	2.73101	24.31848	72.95051
0.00030	2.71731	24.32182	72.96087
0.00031	2.70295	24.32533	72.97171
0.00033	2.68790	24.32901	72.98308
0.00035	2.67210	24.33288	72.99502
0.00036	2.65550	24.33694	73.00756
0.00038	2.63803	24.34122	73.02075
0.00040	2.61961	24.34573	73.03466
0.00042	2.60016	24.35050	73.04934
0.00043	2.57960	24.35554	73.06486

### Composition of C vs Distance



### PROJECT FILE NAME

- Folder: Diffusion Module - DICTRA
- File name: *D\_07\_Diffusion\_Carburization\_Multiphase.tcu*

## Precipitation Calculator Examples



Examples that use three elements are available to all users. The other examples require a Precipitation Module (TC-PRISMA) license to calculate and plot results.



All examples use demonstration database packages included with your installation. You can open the examples from the main menu: **File** → or **Help** → **Examples Files**.



Unless specified in tables for each example, all the numerical parameters are assumed default values.

### *P\_01: Isothermal Precipitation of Al<sub>3</sub>Sc*

This example simulates the kinetics of precipitation of Al<sub>3</sub>Sc from an FCC\_A1 solution phase. The simulation results can be compared with experimental data collected from Marquis and Seidman<sup>1</sup> and Novotny and Ardell (2001)<sup>2</sup>.



This example is available as a video tutorial on [our website](#) and [YouTube channel](#).

System (System Definer)	
Database package	Demo: Aluminum-based alloys (ALDEMO, MALDEMO)
Elements	Al, Sc
Conditions (Precipitation Calculator)	
Composition	Al-0.18Sc Mole percent
Matrix phase	FCC_A1
Precipitate phase	AL3SC
Precipitate Phase Data Parameters (Precipitation Calculator)	
Nucleation sites	Bulk

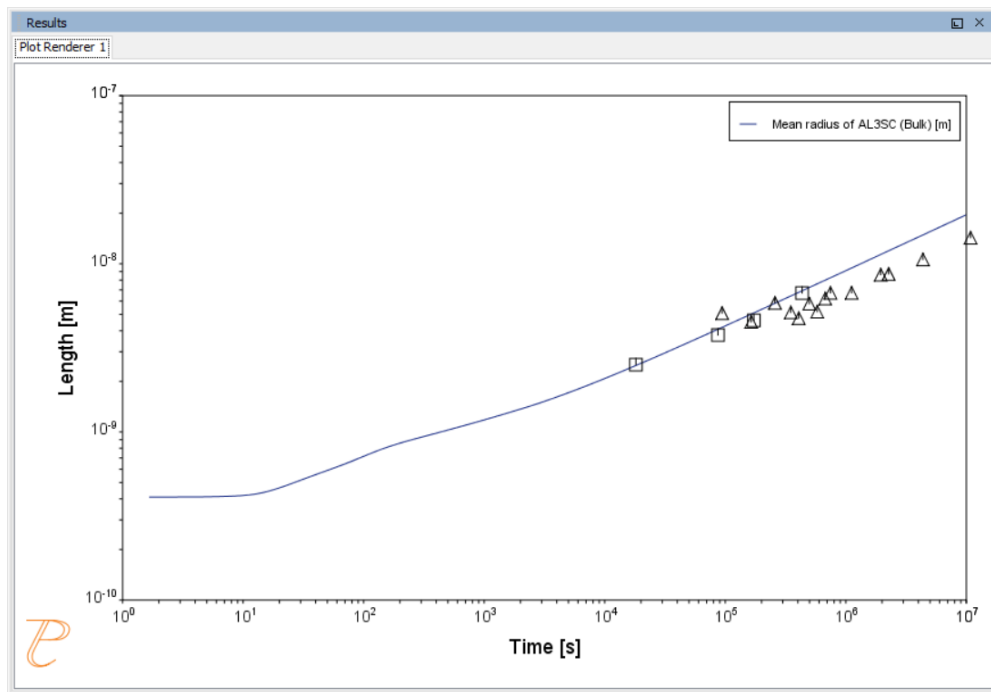
<sup>1</sup>. Marquis, E.A, and D.N Seidman. 2001. "Nanoscale Structural Evolution of Al<sub>3</sub>Sc Precipitates in Al(Sc) Alloys." Acta Materialia 49 (11): 1909–19.

<sup>2</sup>. Novotny, Gabriel M., and Alan J. Ardell. 2001. "Precipitation of Al<sub>3</sub>Sc in Binary Al–Sc Alloys." Materials Science & Engineering, A: Structural Materials: Properties, Microstructure and Processing 318 (1–2): 144–54.

Interfacial energy	Calculated
<b>Calculation Type (Precipitation Calculator)</b>	
Calculation type	Isothermal
Temperature	350° C
Simulation time	1.0E7 seconds
<b>Other</b>	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_01_Precipitation_Al-Sc_AL3SC.tcu

## Plot Results

### Mean radius



## P\_02: Stable and Metastable Carbides - Isothermal



This example simulates the kinetics of precipitation of both stable and metastable carbides from ferrite phase. It demonstrates that metastable carbides (cementite, M7C3) may first emerge and then disappear and the stable phase (M23C6) prevails.

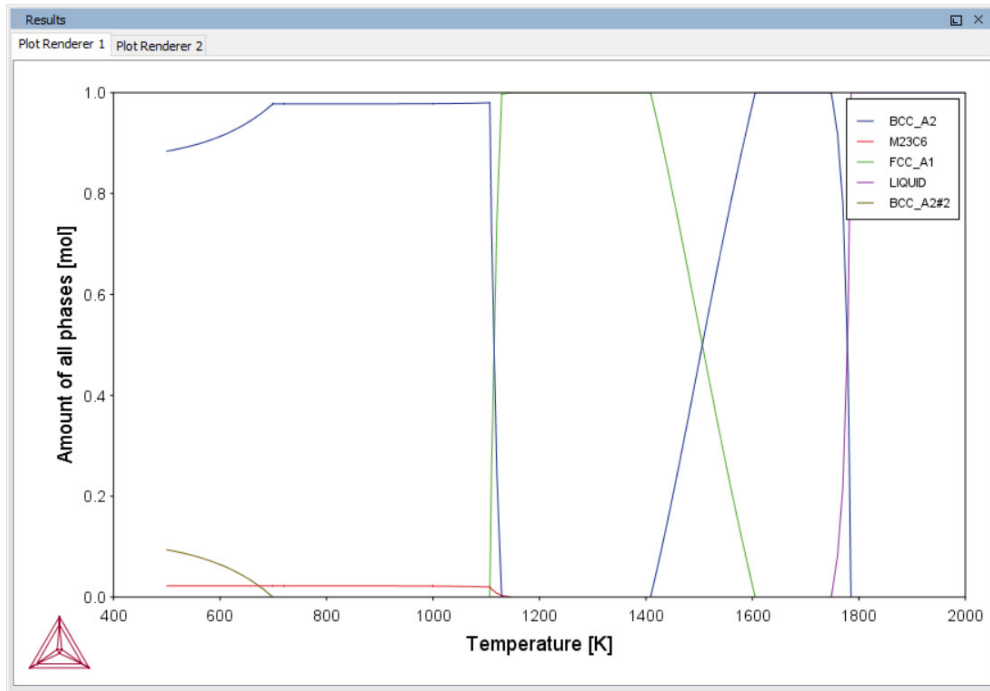
This example uses the Equilibrium Calculator and a property diagram to determine how the phases change with temperature. We are interested in the carbide precipitation at 1053K where only the carbide M23C6 is stable according to the equilibrium calculation. The Precipitation Calculator is used to do an isothermal calculation of the three phases (cementite, M23C6 and M7C3) where cementite and M7C3 are metastable phases.

System (System Definer)	
Database package	Demo: Steels and Fe-alloys (FEDEMO,MFEDEMO)
Elements	Fe, C, Cr
Conditions (Precipitation Calculator)	
Composition	Fe-0.1C-12Cr Mass percent
Matrix phase	BCC_A2
Precipitate phases	Cementite, M23C6 and M7C3
Matrix Phase Data Parameters (Precipitation Calculator)	
Grain size (click <b>Show details</b> to display this setting)	1.0E-4 m
Precipitate Phase Data Parameters (Precipitation Calculator)	
Nucleation sites	Grain boundaries
Interfacial energy	Cementite 0.167 J/m <sup>2</sup> , M23C6 0.252 J/m <sup>2</sup> , M7C3 0.282 J/m <sup>2</sup>
Calculation Type (Precipitation Calculator)	
Calculation type	Isothermal
Temperature	1053 K
Simulation time	400 000 seconds
Other	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_02_Precipitation_Fe-C-Cr_Cementite-M7C3-M23C6.tcu

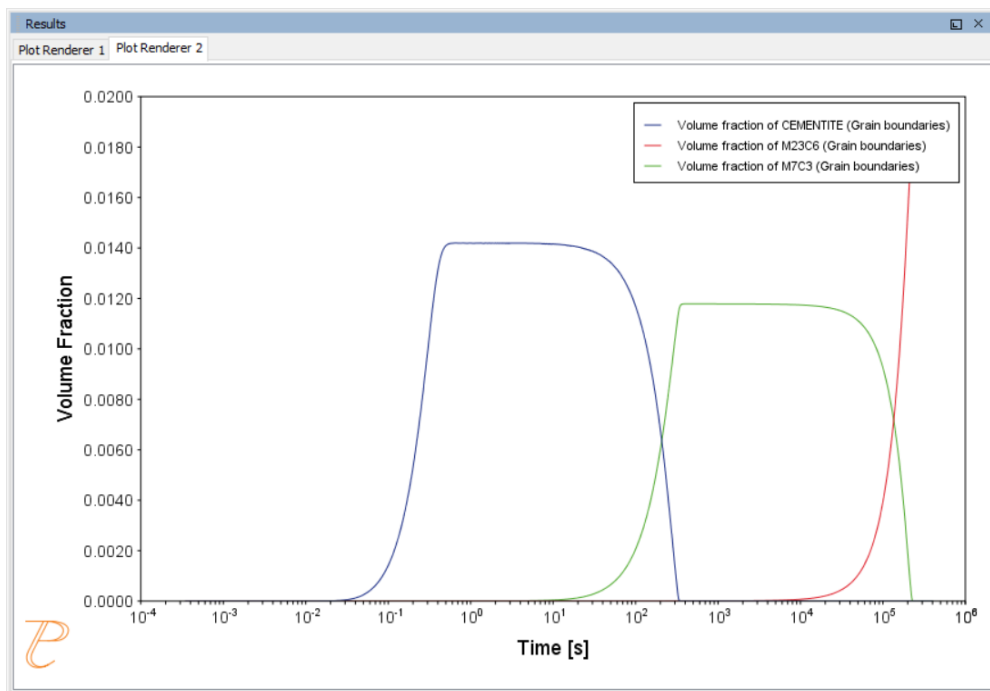


## Plot Results

*Equilibrium Calculator: How the phases change with temperature*



*Precipitation Calculator: Volume fractions*



### P\_03: Stable and Metastable Carbides - TTT Diagram



In this example, the kinetics of precipitation of both stable and metastable carbides is calculated from the ferrite phase. It demonstrates that metastable carbides may first emerge and then disappear and the stable phase prevails.

This example uses the Equilibrium Calculator and a property diagram to determine how the phases change with temperature. Using this result, the Precipitation Calculator is used to do a TTT (Time-Temperature-Transformation) diagram calculation of the three phases (cementite, M23C6 and M7C3) at the grain boundaries.

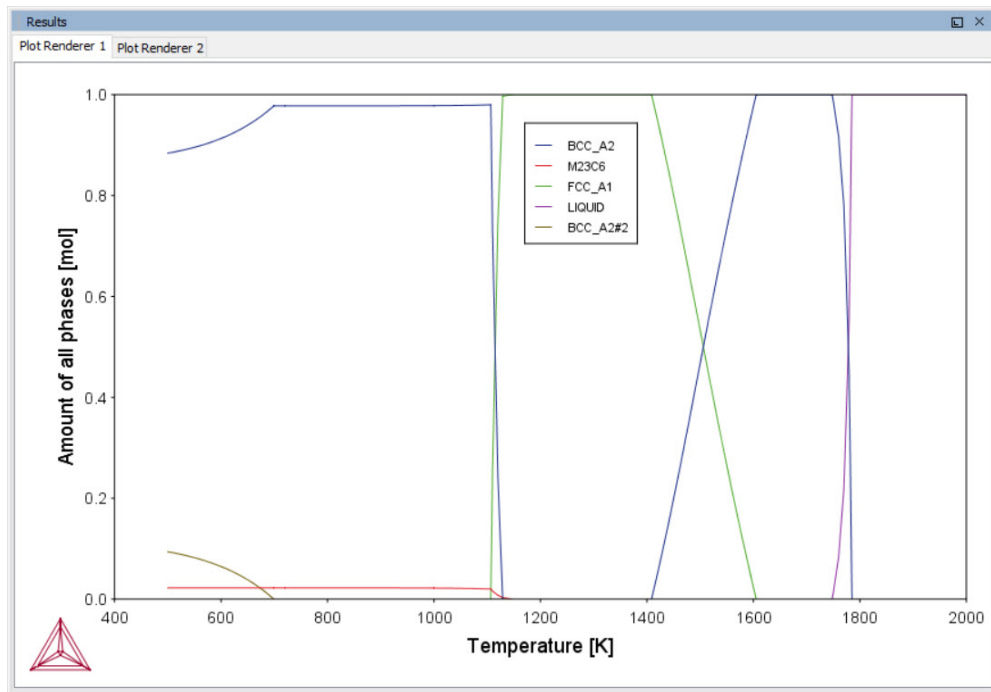
For a TTT diagram calculation, select **TTT diagram** in **Calculation Type**, then enter **Min**, **Max**, and **Step** of **Temperature**, as well as **Max annealing time**. In **Stop criterion**, choose **Volume fraction of phase** and enter the value.

System (System Definer)	
Database package	Demo: Steels and Fe-alloys (FEDEMO and MFEDEMO)
Elements	Fe, C, Cr
Conditions (Precipitation Calculator)	
Composition	Fe-0.1C-12Cr Mass percent
Matrix phase	BCC_A2
Precipitate phases	Cementite, M23C6 and M7C3
Matrix Phase Data Parameters (Precipitation Calculator)	
Grain size (click <b>Show details</b> to display this setting)	1.0E-4 m
Precipitate Phase Data Parameters	
Nucleation sites	Grain boundaries
Interfacial energy	Cementite 0.167 J/m <sup>2</sup> , M23C6 0.252 J/m <sup>2</sup> , M7C3 0.282 J/m <sup>2</sup>
Calculation Type (Precipitation Calculator)	
Calculation type	TTT diagram
Temperature	500° to 800° C with 25° C steps

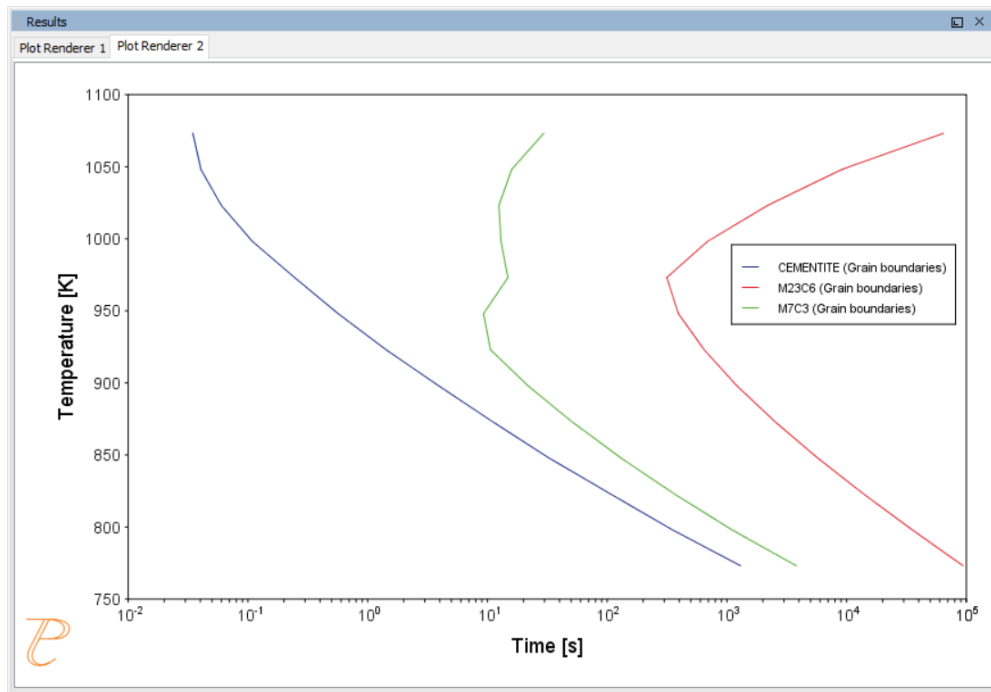
Max. annealing time	1.0E8 seconds
Stop criteria	Volume fraction of phase is set to 0.0001
<b>Other</b>	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_03_Precipitation_Fe-C-Cr_TTT_Cementite-M7C3-M23C6.tcu

## Plot Results

*Equilibrium Calculator: How the phases change with temperature*



### Precipitation Calculator: TTT diagram



### P\_04: Precipitation of Iron Carbon Cementite

Simulate the kinetics of precipitation of carbides from a BCC Fe solution phase. This example is based on Wert (1949)<sup>1</sup>.

This example uses two Experimental File Reader activities with the Precipitation Calculator and an isothermal calculation, to plot the volume fraction of the cementite phase.

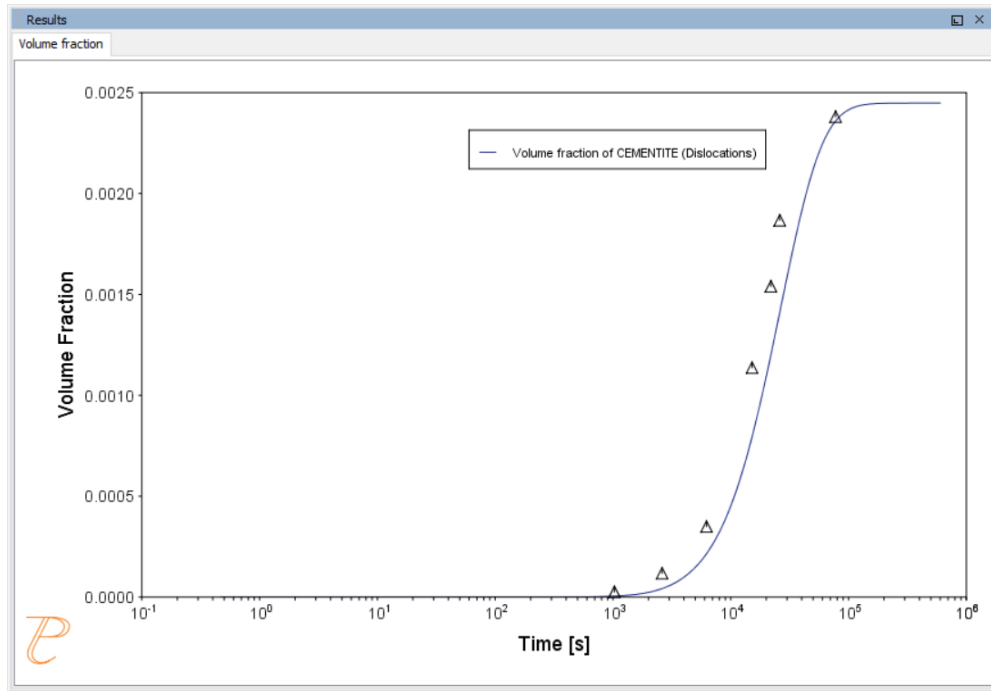
System (System Definer)	
Database package	Demo: Steels and Fe-alloys (FEDEMO and MFEDEMO)
Elements	Fe, C
Conditions (Precipitation Calculator)	
Composition	Fe-0.016C mass percent
Matrix phase	BCC_A2

<sup>1</sup>. Wert, Charles A. 1949. "Precipitation from Solid Solutions of C and N in  $\alpha$ -Iron." Journal of Applied Physics 20 (10). AIP Publishing: 943.

Precipitate phase	Cementite
<b>Matrix Phase Data Parameters (Precipitation Calculator)</b>	
Grain aspect ratio (click <b>Show details</b> to display this setting)	1.0
Dislocation density (click <b>Show details</b> to display this setting)	$1.5 \times 10^{11} \text{m}^{-3}$
<b>Precipitate Phase Parameters (Precipitation Calculator)</b>	
Nucleation sites	Dislocations
Interfacial energy	$0.24 \text{ J/m}^2$
<b>Calculation Type (Precipitation Calculator)</b>	
Calculation type	Isothermal
Temperature	$102^\circ \text{C}$
Simulation time	600 000 seconds
<b>Options (Precipitation Calculator)</b>	
Growth rate model	Advanced
<b>Other</b>	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_04_Precipitation_Fe-C_Cementite.tcu

## Plot Results

### Volume Fraction



### P\_05: Precipitation of $\gamma'$ in Ni Superalloys - Isothermal



This example simulates the kinetics of precipitation of  $\gamma'$  phase from  $\gamma$  phase. The simulation results can be compared with experimental data collected from Sudbrack et al. (2008)<sup>1</sup>.

This example uses three Experimental File Reader activities with the Precipitation Calculator. It does an isothermal calculation to plot the volume fraction, mean radius and number density of the cementite phase.



DIS\_FCC\_A1 needs to be selected on the System Definer. Search the online help for **Selecting the Disordered Phase as a Matrix Phase** in the *Precipitation Module (TC-PRISMA) User Guide* for details.

#### System (System Definer)

Database package

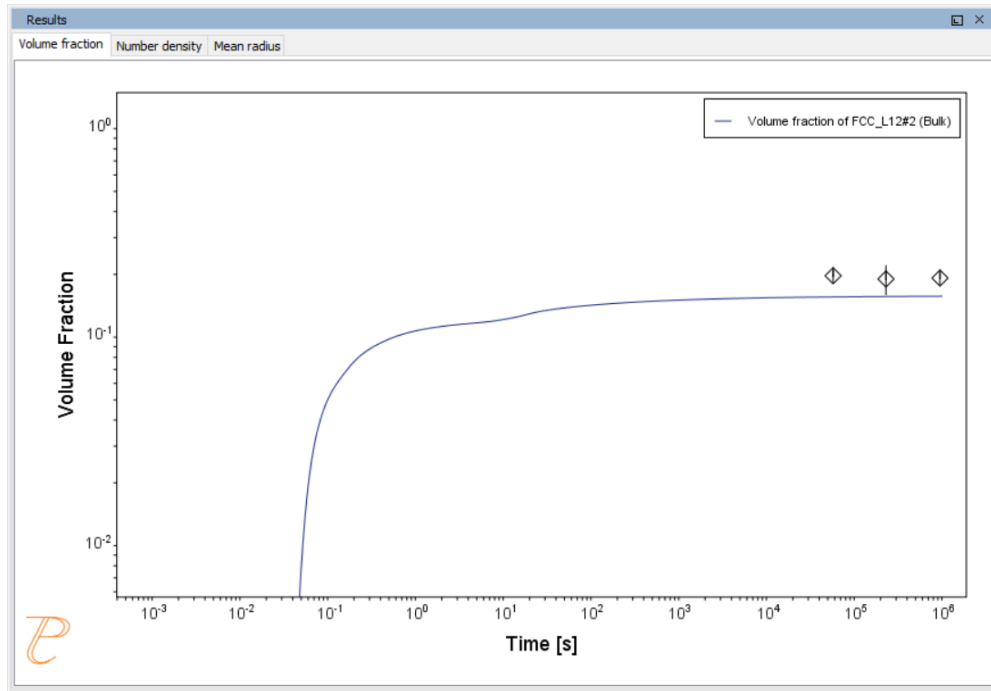
Demo: Nickel-based Super Alloys (NIDEMO and MNIDEMO)

<sup>1</sup> Sudbrack, Chantal K., Tiffany D. Ziebell, Ronald D. Noebe, and David N. Seidman. 2008. "Effects of a Tungsten Addition on the Morphological Evolution, Spatial Correlations and Temporal Evolution of a Model Ni–Al–Cr Superalloy." *Acta Materialia* 56 (3): 448–63.

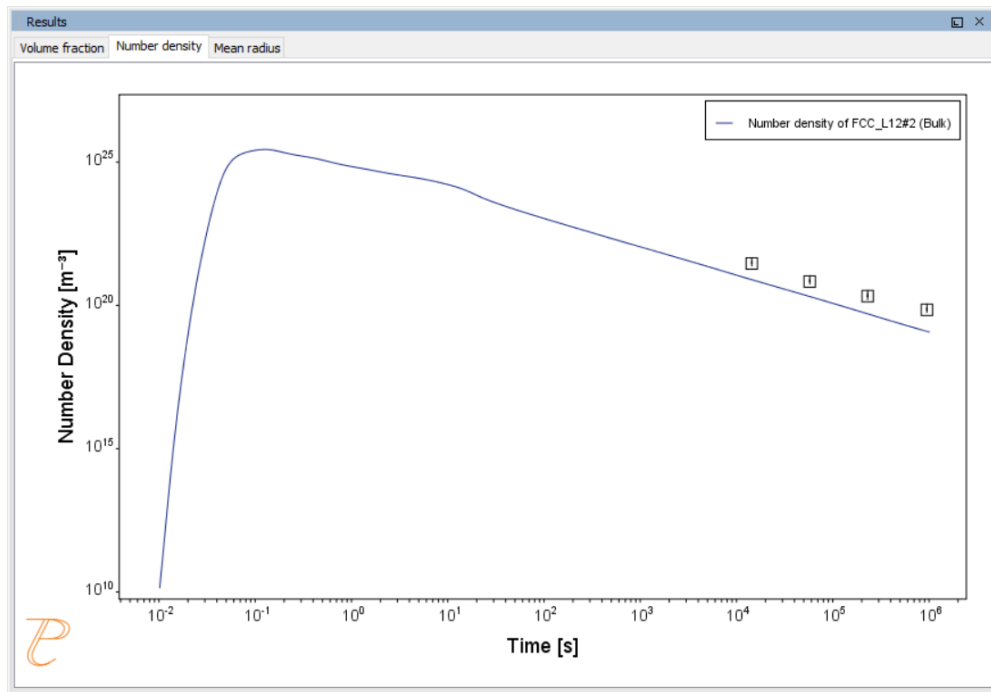
Elements	Ni, Al Cr
<b>Conditions (Precipitation Calculator)</b>	
Composition	Ni-9.8Al-8.3Cr Mole percent
Matrix phase	DIS-FCC_A1 (see note above about how to select this phase)
Precipitate phase	FCC_L12#2
<b>Precipitate Phase Data Parameters (Precipitation Calculator)</b>	
Nucleation sites	Bulk
Interfacial energy	0.012 J/m <sup>2</sup>
<b>Calculation Type (Precipitation Calculator)</b>	
Calculation type	Isothermal
Temperature	800° C
Simulation time	1 000 000 seconds
<b>Other</b>	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_05_Precipitation_Ni-Al-Cr_Isothermal_Gamma-Gamma_prime.tcu

## Plot Results

### Volume Fraction

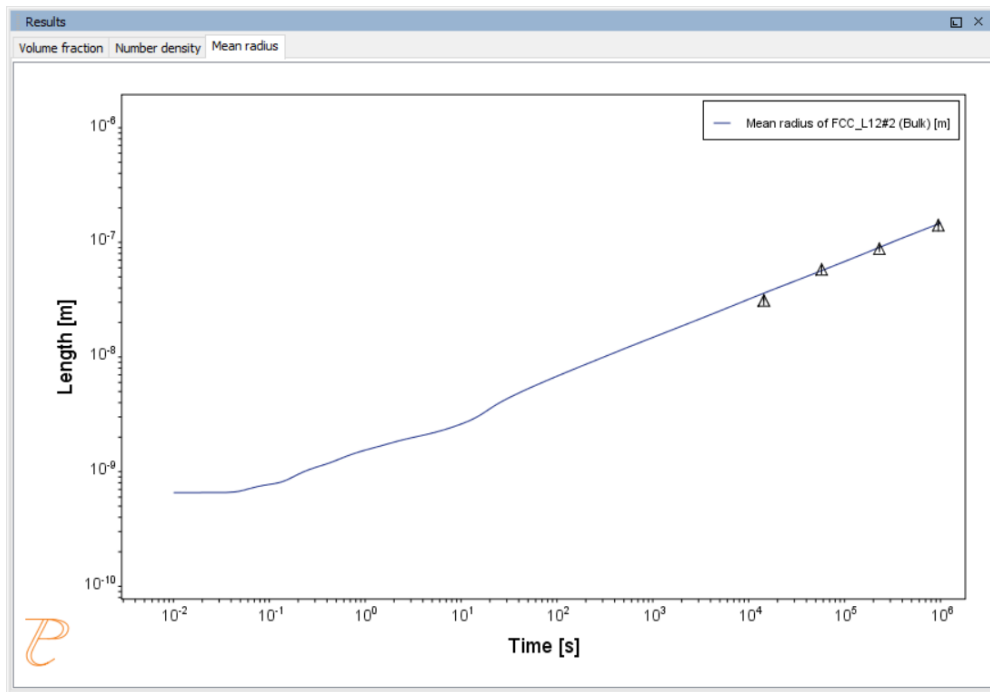


### Number Density





## Mean Radius



### P\_06: Precipitation of $\gamma'$ in Ni Superalloys - Non-isothermal

P

This example simulates the kinetics of precipitation of  $\gamma'$  phase from  $\gamma$  phase in Ni-8Al-8Cr and Ni-10Al-10Cr at.% alloys during continuous cooling. The simulation results can be compared with experimental results from Rojhirunsakool et al. (2013)<sup>1</sup>.

P

When you run (Perform) this example, it takes about 10 minutes for the calculations to complete.

In these examples a linear, continuously cooling condition is set up. This is done on the Precipitation Calculator settings window in the **Calculation Type** section:

1. Select a **Non-Isothermal**.
2. Select a **Temperature Unit** and **Time Unit** from the lists.
3. Click **Thermal Profile**, where **Time-Temperature** profile points are entered to describe the stepwise heat treatment schedule with linear segments. Up to 999 rows of data

<sup>1</sup>. Rojhirunsakool, Tanaporn, S. Meher, J. Y. Hwang, S. Nag, J. Tiley, and Rajarshi Banerjee. 2013. "Influence of Composition on Monomodal versus Multimodal  $\gamma'$  Precipitation in Ni–Al–Cr Alloys." Journal of Materials Science 48 (2): 825–31.

points can be entered.

In these examples two rows of data points are needed for starting time 0s and temperature 1150° C, as well as end time 3300s and temperature 380° C.

- Click the **Plot Renderer** node to select the **Separate multimodal PSD** check box. This plots the mean radius and size distributions of the two compositions.

Plotting the size distribution from the final simulation time of 3300 seconds, you can see there are several peaks, although these are not completely separated. As above, select the **Separate multimodal PSD** check box to separate the peaks.

- Adjust the **Valley depth ratio** setting to 0.05 to separate into two peaks as shown in the [Ni-10Al-10Cr plot example](#). You can experiment with this setting to see how the size distribution evolves with time, for example, try entering several values as plot times **400 600 3300**.



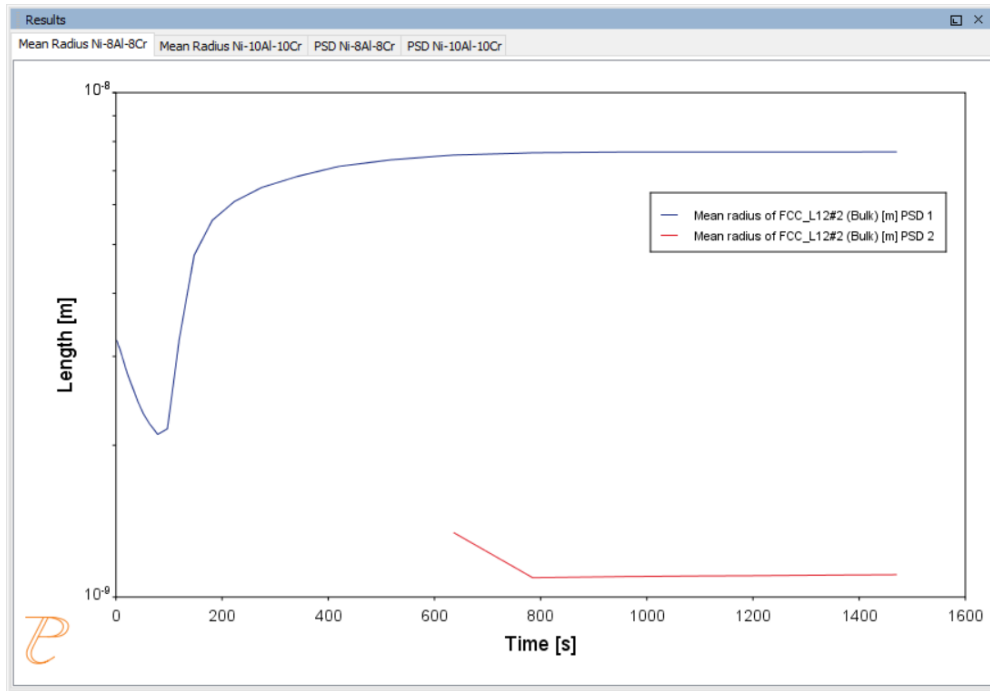
DIS\_FCC\_A1 needs to be selected on the System Definer. Search the online help for **Selecting the Disordered Phase as a Matrix Phase** in the *Precipitation Module (TC-PRISMA) User Guide* for details.

System (System Definer)	
Database package	Demo: Nickel-based Super Alloys (NIDEMO and MNIDEMO)
Elements	Ni, Al, Cr
Conditions (Precipitation Calculator)	
Composition (Ni-8Al-8Cr)	Ni-8Al-8Cr Mole percent
Composition (Ni-10Al-10Cr)	Ni-10Al-10Cr Mole percent
Matrix phase	DIS_FCC_A1 (see note above about how to select this phase)

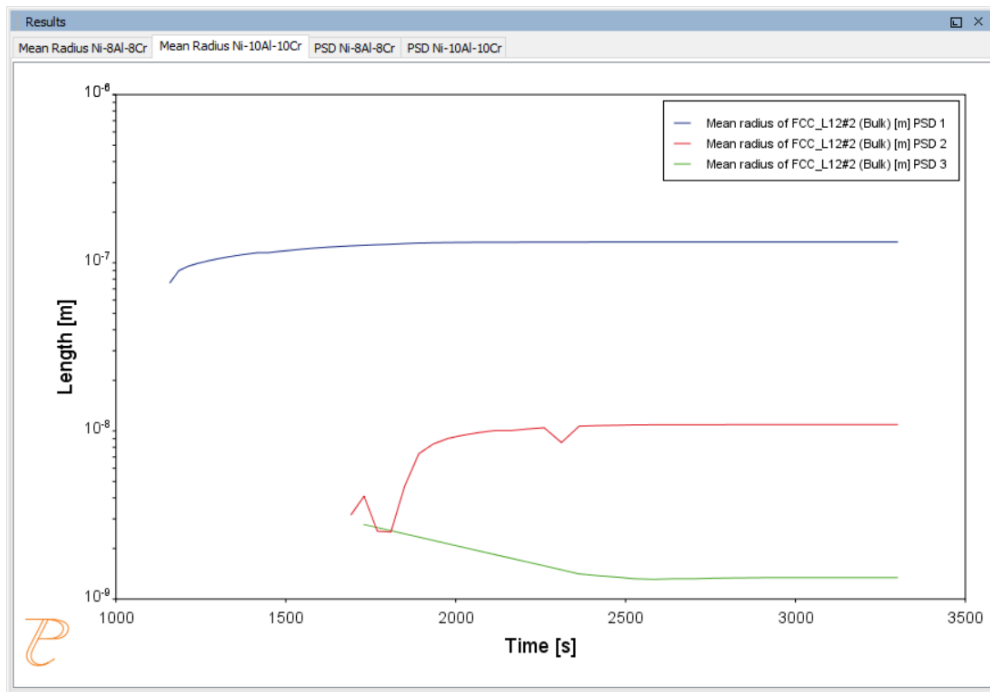
Precipitate phase	FCC_L12#2
<b>Matrix Phase Data Parameters (Precipitation Calculator)</b>	
Mobility enhancement prefactor (click <b>Show details</b> to display this setting)	5.0
<b>Precipitate Phase Data Parameters (Precipitation Calculator)</b>	
Nucleation sites	Bulk
Interfacial energy	0.023 J/m <sup>2</sup>
<b>Calculation Type (Precipitation Calculator)</b>	
Calculation type	Non-isothermal
Temperature unit	Celsius
Time unit	Seconds
Simulation time (Ni-8Al-8Cr)	1470 s
Simulation time (Ni-10Al-10Cr)	3300 s
<b>Multimodal PSD (Plot Renderer)</b>	
Separate multimodal PSD for 8Al-8Cr	The <b>Valley depth ratio</b> is set to 0.05 for both plots. The number of <b>Points</b> is increased to 200 for an average radius plot.
Separate multimodal PSD for 10Al-10Cr	The <b>Valley depth ratio</b> is set to 0.18 for both plots.
<b>Other</b>	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_06_Precipitation_Ni-Al-Cr_Non-isothermal_Gamma-Gamma_prime.tcu

## Plot Results

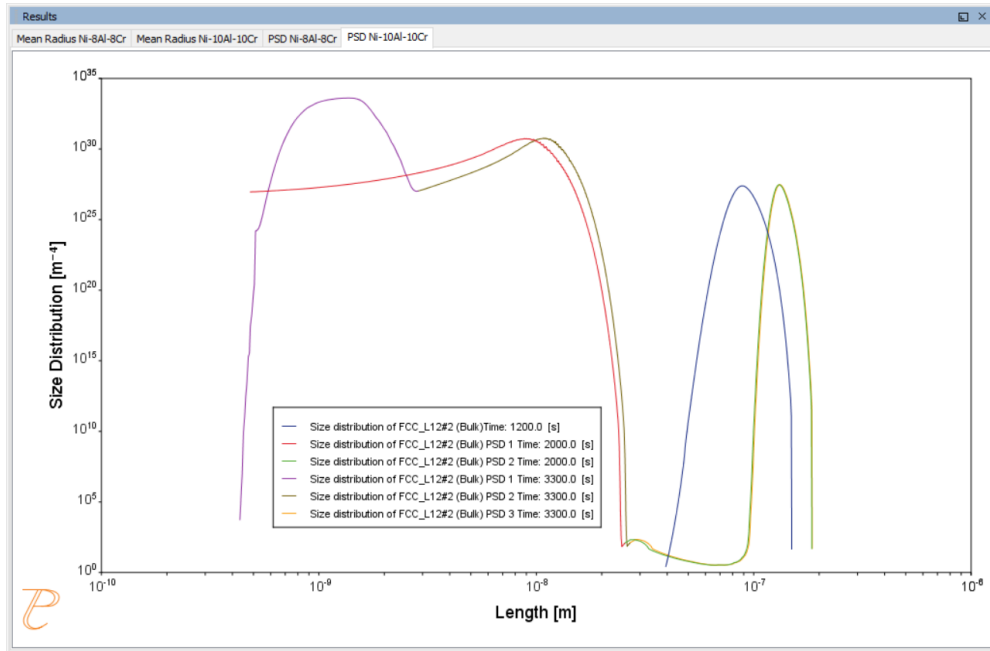
### Mean Radius Ni-8Al-8Cr



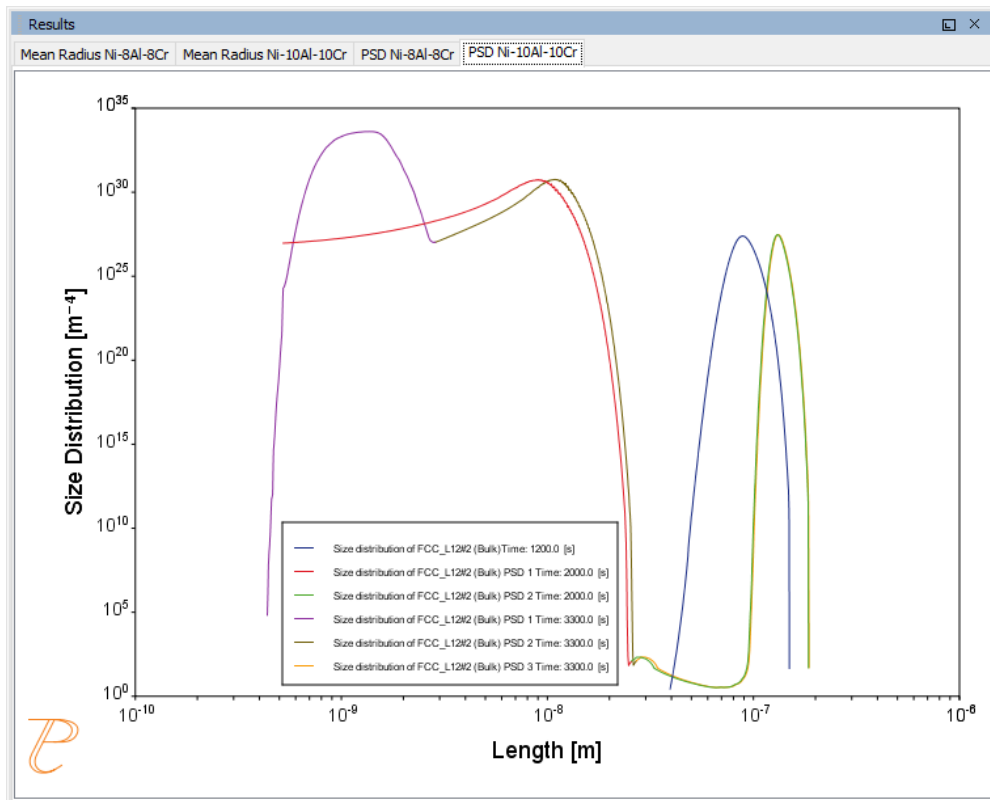
### Mean Radius Ni-10Al-10Cr



## Size Distribution (PSD) Ni-8Al-8Cr



## Size Distribution (PSD) Ni-10Al-10Cr

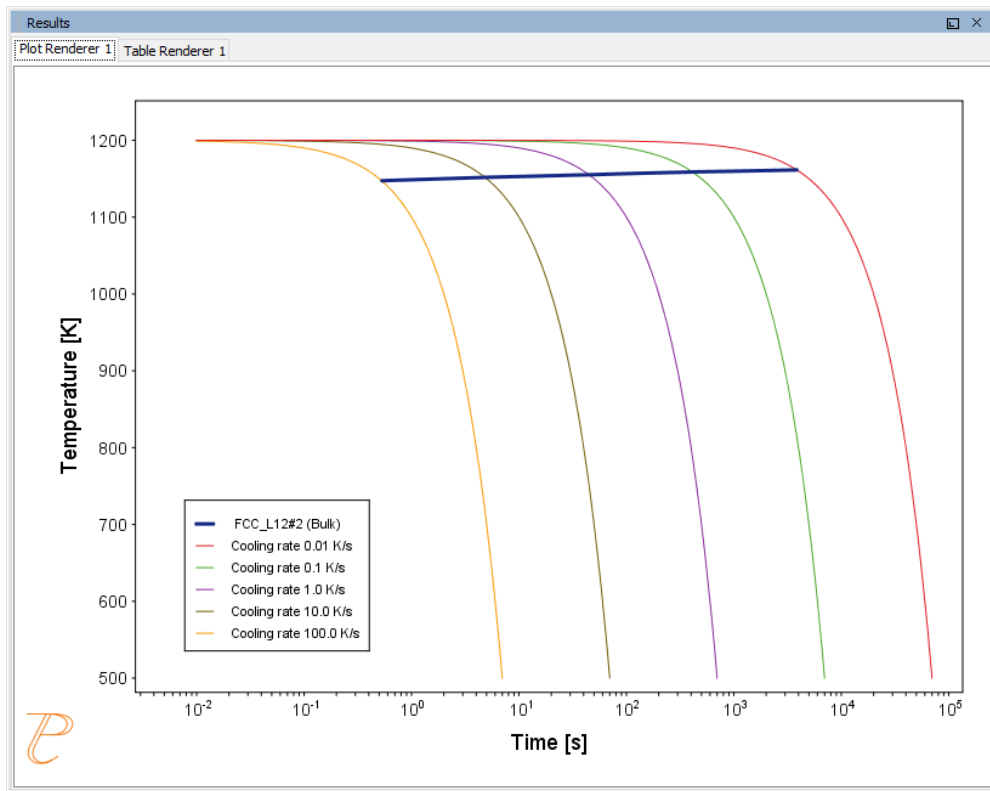


***P\_07: Cooling Rate (CCT) Diagram of Ni-Al-Cr  $\gamma$ - $\gamma'$*** 

In this example, a CCT diagram for a Ni-10Al-10Cr  $\gamma$ - $\gamma'$  alloy is calculated and plotted with superimposition of the cooling rate values.

System (System Definer)	
Database package	Demo: Nickel-based Super Alloys (NIDEMO and MNIDEMO)
Elements	Ni, Al, Cr
Conditions (Precipitation Calculator)	
Composition	Ni-10Al-10Cr Mole percent
Matrix phase	DIS_FCC_A1
Precipitate phase	FCC_L12#2
Precipitate Phase Data Parameters (Precipitation Calculator)	
Nucleation sites	Bulk
Interfacial energy	0.023 J/m <sup>2</sup>
Calculation Type (Precipitation Calculator)	
Calculation type	CCT Diagram
Temperature Min to Max	500 to 1200 Kelvin
Cooling rate(s)	.01 .1 1 10 100 K/s
Stop criteria	Volume fraction of phase 1.0E-4
Other	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_07_Precipitation_Ni-Al-Cr_CCT_Gamma-Gamma_prime.tcu

## Plot and Table Results



Results	
Plot Renderer 1	Table Renderer 1
Temperature [K]	FCC_L12#2 (Bulk)
1147.52034	0.53291
1151.74192	4.83553
1155.24636	44.76534
1158.85368	411.49173
1161.48750	3851.47779

### *P\_08: Precipitation of Cu-Ti CU4Ti1 with Assumptions of Sphere and Needle Morphologies*

In this isothermal calculation example, the precipitation of Cu<sub>4</sub>Ti phase in a Cu-Ti binary alloy is calculated. To make a comparison, two separate simulations are performed, one assuming spherical morphology without elastic strain energy, and the other assuming needle morphology whose shape, determined by competition between interfacial energy and elastic strain energy,

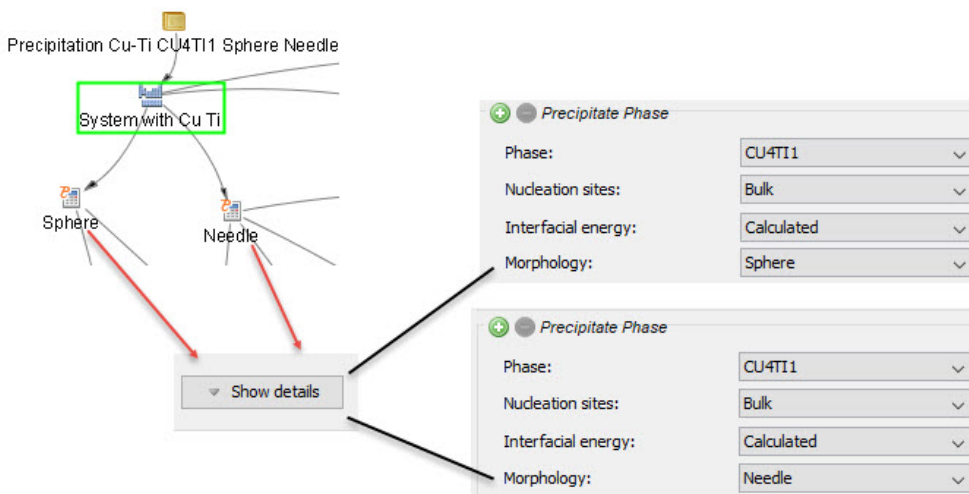
is changed during the simulation. The transformation strain is obtained from Borchers<sup>1</sup>. The results are compared with experiment results from Kampmann et al<sup>2</sup>.

This example takes a few minutes to run.



To ensure that the settings are done on the correct Precipitation Calculators, the **Sphere** and **Needle** nodes are renamed from **Precipitation Calculator** to match their morphology. The morphology is set in the **Precipitate Phase** section when you click **Show details**.

► Search the help for "precipitation morphology".



### System (System Definer)

Database package	Demo: Copper-based alloys (CUDEMO and MCUDEMO)
Elements	Cu, Ti

### Sphere and Needle Conditions (Precipitation Calculator)

Composition	Cu-1.9Ti Mole percent
Matrix phase	FCC_L12

<sup>1</sup>. Borchers C. 1999. "Catastrophic Nucleation during Decomposition of Cu-0.9at.%Ti." Phil. Mag. A 79(3):537-547

<sup>2</sup>. Kampmann R., Eckerlebe H., and Wagner R. 1987. "Precipitation Kinetics in Metastable Solid Solutions - Theoretical Considerations and Application to Cu-Ti Alloys." Mat. Res. Soc. Symp. Proc. 57: 525-542.

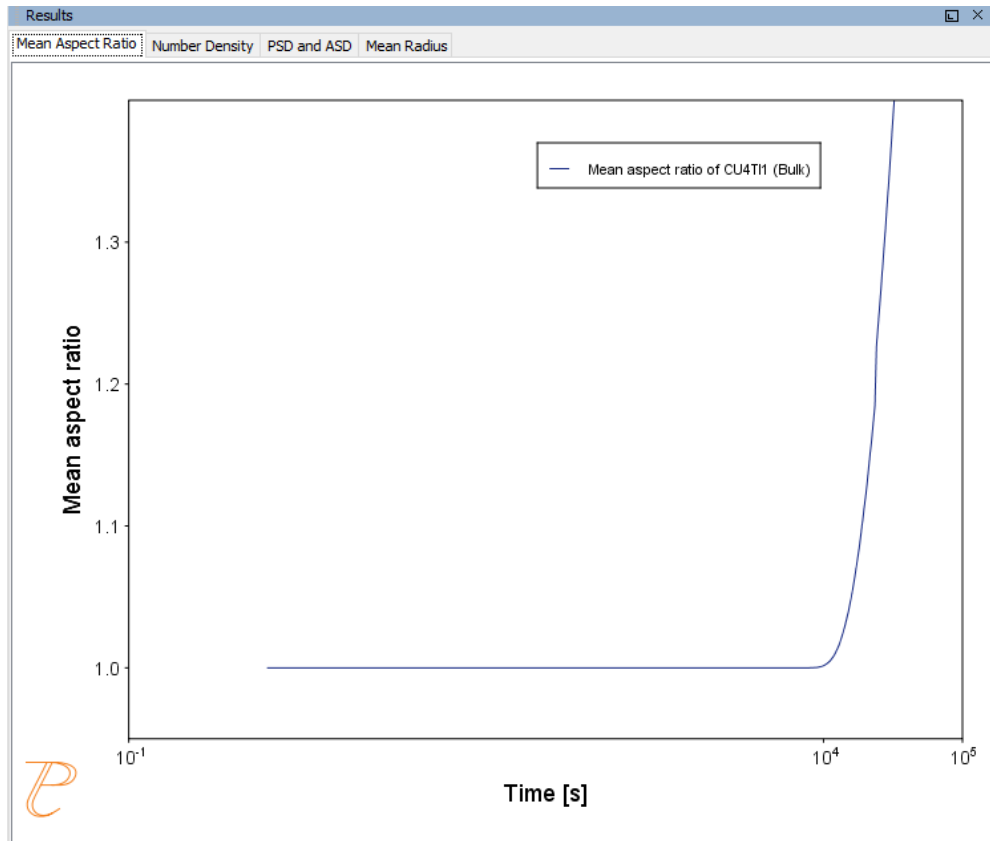


Precipitate phase	CU4Ti1
<b>Matrix Phase Data Parameters (Precipitation Calculator)</b>	
Mobility enhancement prefactor (click <b>Show details</b> to display this setting)	100
<b>Precipitate Phase Data Parameters (Precipitation Calculator)</b>	
Nucleation sites	Bulk
Interfacial energy	The default
Morphology (click <b>Show details</b> to display this setting)	<p>For the <b>Sphere</b> node (renamed from Precipitation Calculator), keep the default.</p> <p>For the <b>Needle</b> node (renamed from Precipitation Calculator), <b>Needle</b> is selected.</p>
Transformation strain (click <b>Show details</b> to display this setting)	<p>For the <b>Sphere</b> node (renamed from Precipitation Calculator), keep the default.</p> <p>For the <b>Needle</b> node (renamed from Precipitation Calculator), <b>User defined</b> is selected. In this example, the following settings are defined:</p> <ul style="list-style-type: none"> <li>• <math>\epsilon_{11}</math> and <math>\epsilon_{22}</math> are set to <b>0.022</b></li> <li>• <math>\epsilon_{33}</math> is set to <b>0.003</b></li> </ul>
<b>Calculation Type (Precipitation Calculator)</b>	
Calculation type	Isothermal
Temperature	350° C
Simulation time	10,000 seconds
<b>Datasets (Experimental File Reader)</b>	
Borchers Mean radius vs Time and Borchers Number density vs Time	Data sets included with this example and imported to two Experimental File Readers. These data sets are used for the Mean Radius and Number Density plots, respectively.
<b>Other</b>	
File name and location	Folder: Precipitation Module - TC-PRISMA

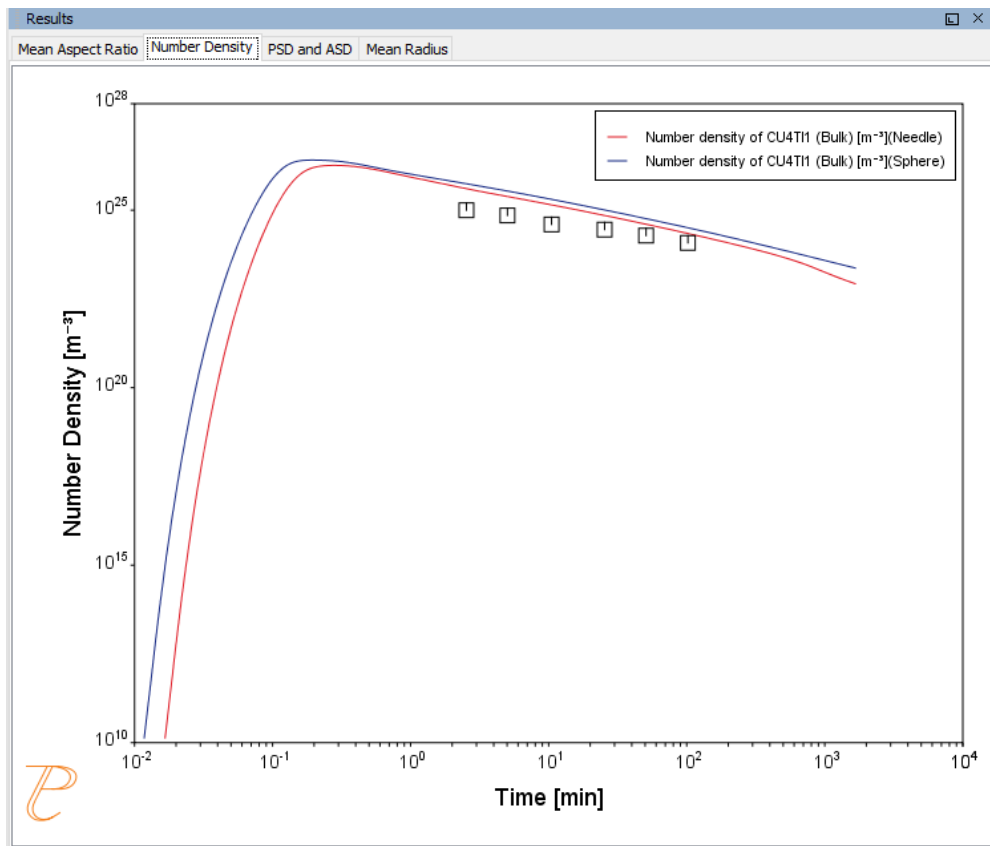
File name: P\_08\_Precipitation\_Cu-Ti\_CU4Ti1\_Sphere\_Needle.tcu

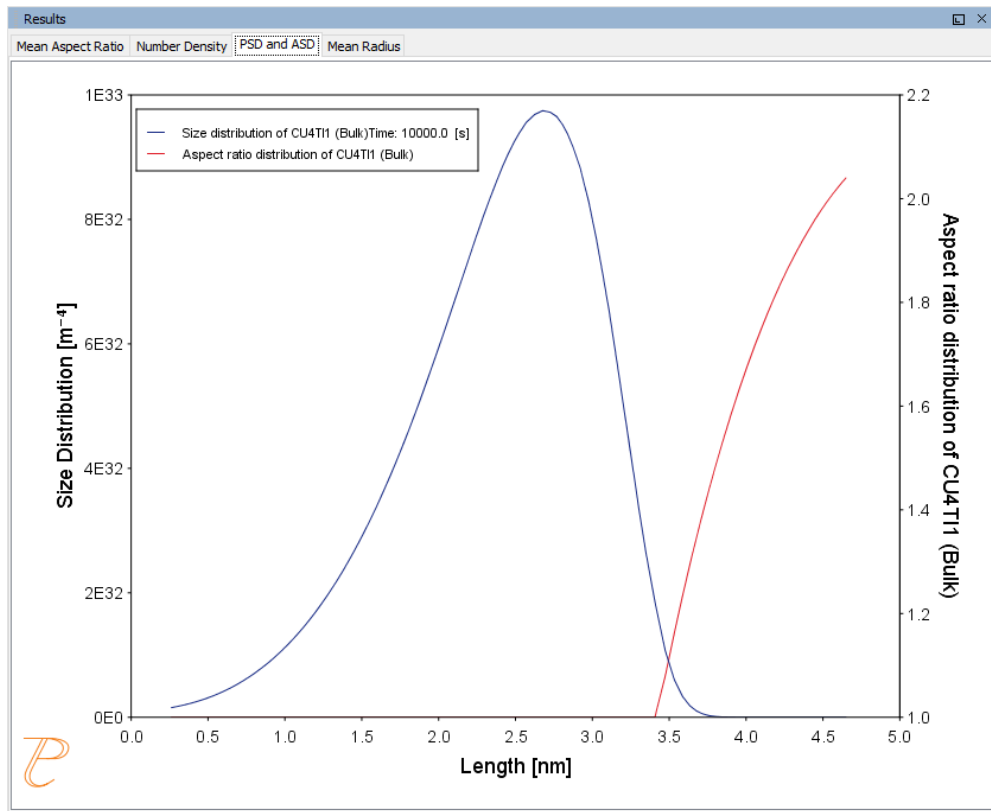
## Plot Results

### Mean Aspect Ratio

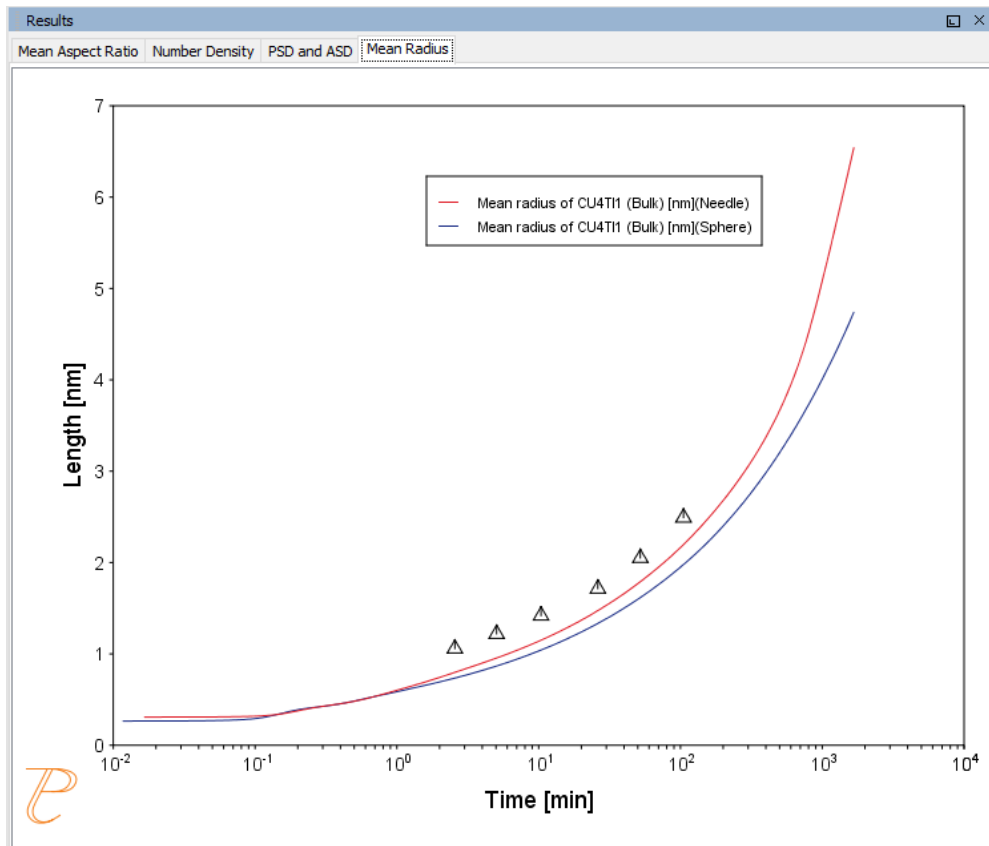


## Number Density



*PSD and ASD*

## Mean Radius



### ***P\_09: Precipitation of Al-Sc Al<sub>3</sub>Sc with Assumption of Sphere and Cuboid Morphologies***

In this isothermal calculation example, the precipitation of Al<sub>3</sub>Sc phase from FCC\_A1 matrix phase in an Al-Sc binary alloy is simulated. To make a comparison, two separate calculations are performed, one assuming spherical morphology without elastic strain energy, and the other assuming cuboid morphology whose shape is determined by competition between interfacial energy and elastic strain energy. The simulation results are compared with experimental data collected from Marquis and Seidman<sup>1</sup> and Novotny and Ardell (2001)<sup>2</sup>. In addition, mean cubic factor and cubic factor distribution are also plotted for cuboid shape to illustrate the spherical-cuboidal transition during precipitation.

<sup>1</sup>. Marquis, E.A, and D.N Seidman. 2001. "Nanoscale Structural Evolution of Al<sub>3</sub>Sc Precipitates in Al(Sc) Alloys." *Acta Materialia* 49 (11): 1909–19.

<sup>2</sup>. Novotny, Gabriel M., and Alan J. Ardell. 2001. "Precipitation of Al<sub>3</sub>Sc in Binary Al–Sc Alloys." *Materials Science & Engineering, A: Structural Materials: Properties, Microstructure and Processing* 318 (1–2): 144–54.



To ensure that the settings are done on the correct Precipitation Calculators, the **Sphere** and **Cuboid** nodes are renamed from **Precipitation Calculator** to match their morphology. The morphology is set in the **Precipitate Phase** section when you click **Show details**. See P\_08 for an example of this.

► Search the help for "precipitation morphology".

#### System (System Definer)

Database package	Demo: Aluminum-based alloys (ALDEMO, MALDEMO)
Elements	Al, Sc

#### Sphere and Cuboid Conditions (Precipitation Calculator)

Composition	Al-0.18Sc Mole percent
Matrix phase	FCC_A1
Precipitate phase	AL3SC

#### Matrix Phase Data Parameters (Precipitation Calculator)

Elastic properties (click <b>Show details</b> to display this setting)	<p>For the <b>Sphere</b> node (renamed from Precipitation Calculator), the default, <b>Disregard</b> is kept.</p> <p>For the <b>Cuboid</b> node (renamed from Precipitation Calculator), choose <b>Cubic</b>. Then enter the elastic constants accordingly. Default elastic constants are given based on the major element of the alloy system. In this example that is</p> <ul style="list-style-type: none"> <li>• c11 is <b>108.2</b> GPa</li> <li>• c12 is <b>61.3</b> GPa</li> <li>• c44 is <b>28.5</b> GPa</li> </ul>
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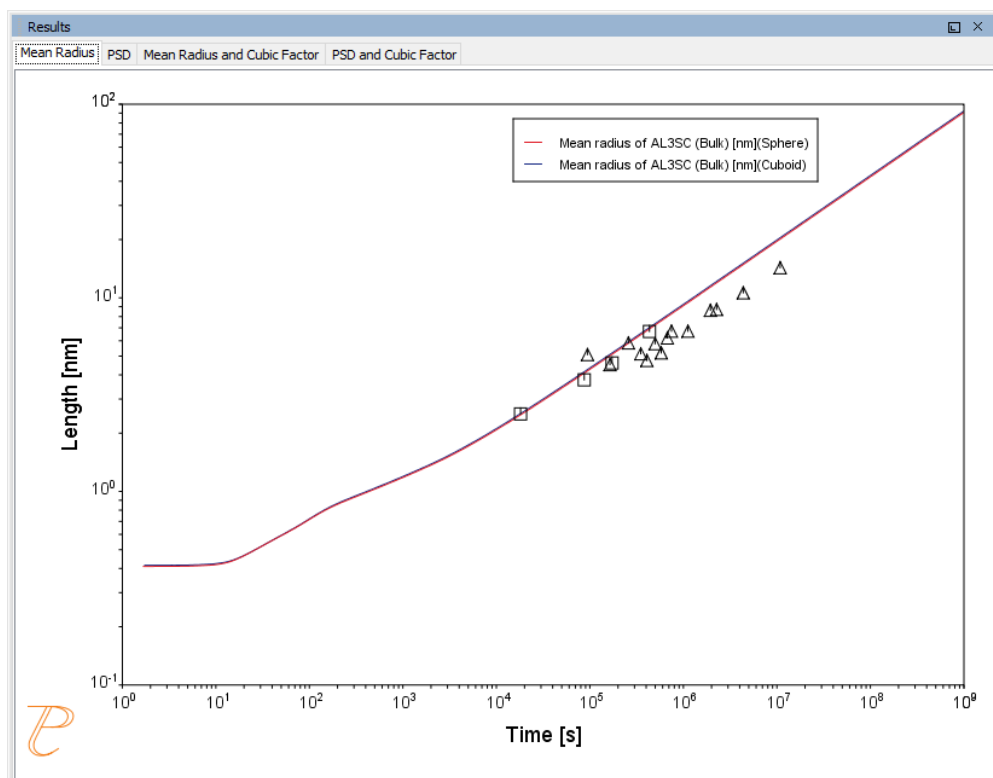
#### Precipitate Phase Data Parameters (Precipitation Calculator)

Nucleation sites	Bulk
Interfacial energy	The default
Morphology (click <b>Show details</b> to display this setting)	<p>For the <b>Sphere</b> node (renamed from Precipitation Calculator), keep the default.</p> <p>For the <b>Cuboid</b> node (renamed from Precipitation Calculator), <b>Cuboid</b> is selected.</p>
Transformation strain (click <b>Show details</b> to display this setting)	For the <b>Sphere</b> node (renamed from Precipitation Calculator), keep the default.

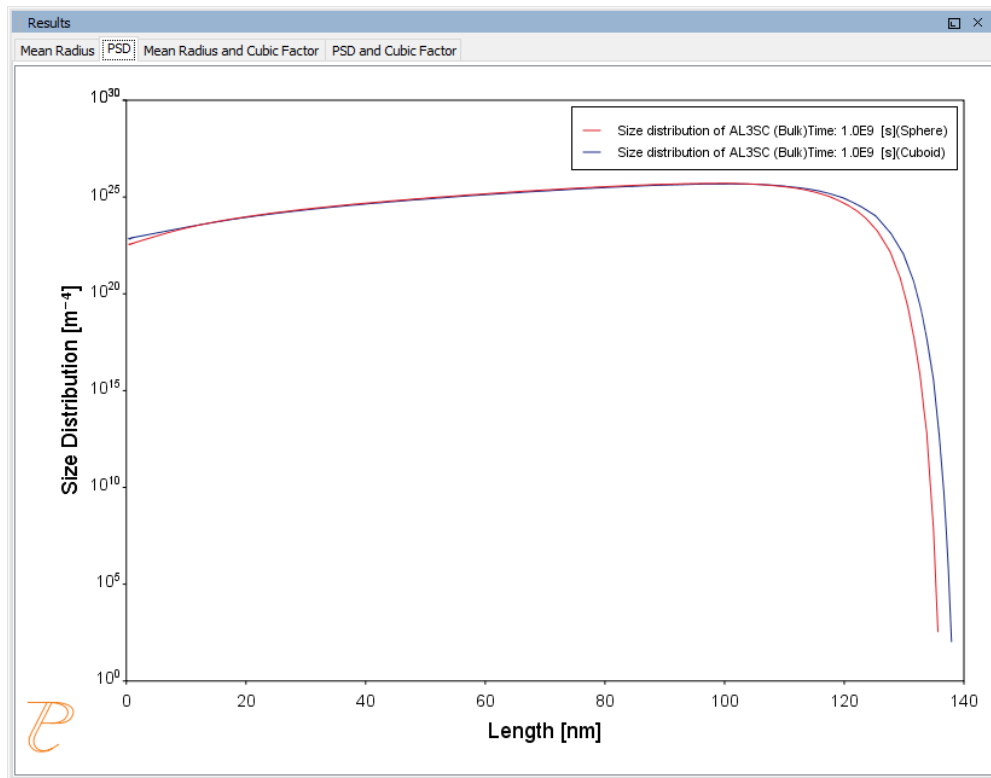
display this setting)	For the <b>Cuboid</b> node (renamed from Precipitation Calculator), <b>Calculate from molar volume</b> is selected to obtain a purely dilatational strain.
<b>Calculation Type (Precipitation Calculator)</b>	
Calculation type	Isothermal
Temperature	350° C
Simulation time	1.0E9 seconds
<b>Datasets (Experimental File Reader)</b>	
Dataset 1 and Dataset 2	Data sets included with this example and imported to one Experimental File Reader. It is used for the Mean Radius plot.
<b>Other</b>	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_09_Precipitation_Al-Sc_AL3SC_Sphere_Cuboid.tcu

## Plot Results

### Mean Radius

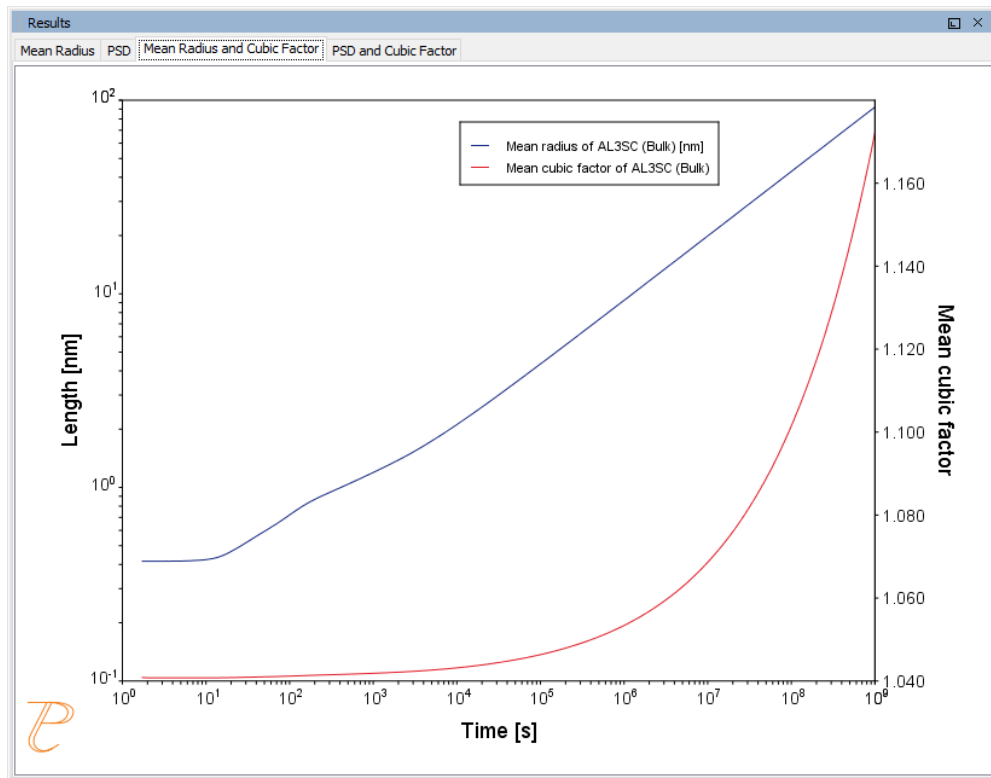


## PSD

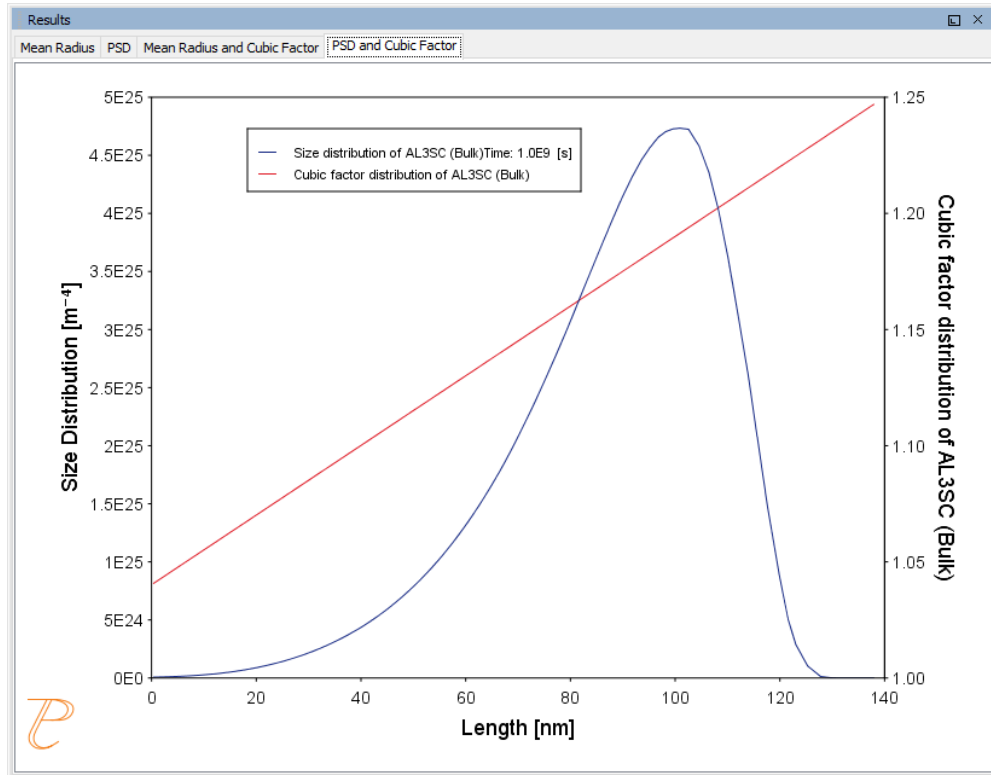




### Mean Radius and Cubic Factor



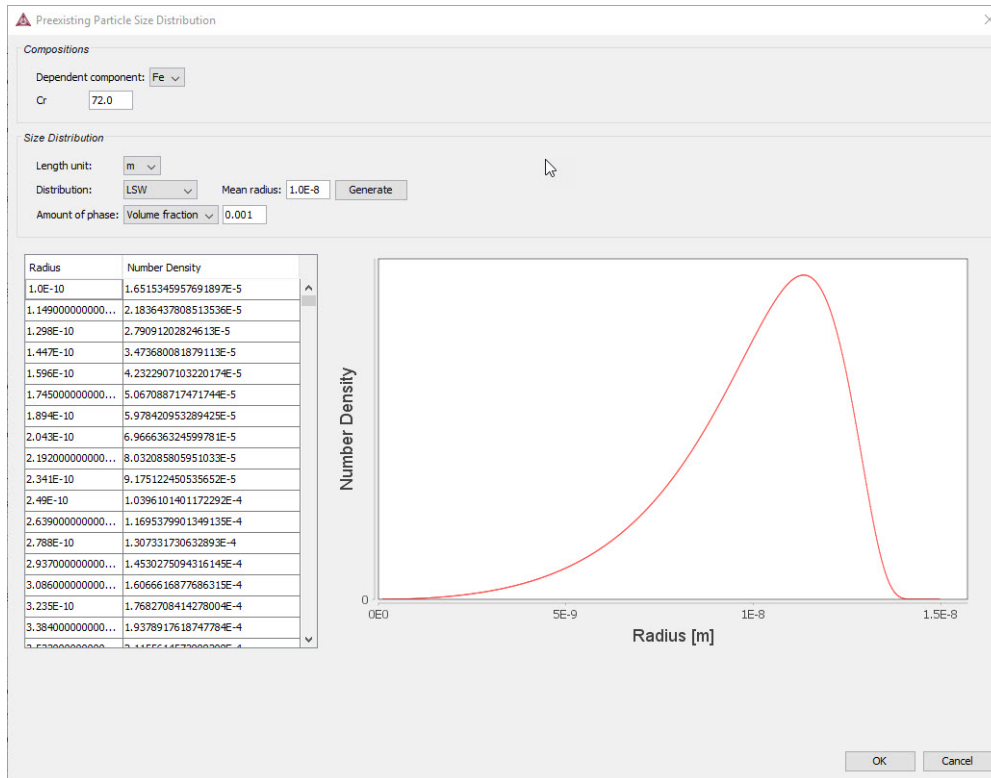
## PSD and Cubic Factor



### P\_10: Initial Particle Size Distribution of Fe-Cr-C

This example demonstrates the effect of initial particle size distribution of the precipitate phases on the overall precipitation kinetics. It uses two Precipitation Calculators to simulate and compare carbide precipitations from a ferritic BCC\_A2 matrix in a Fe-0.1C-12Cr alloy. Three carbides, CEMENTITE, M23C6 and M7C3, are included in the calculations for competitive precipitations, and the precipitation kinetics are compared with or without initial particle size distribution.

The example illustrates the use of the particle size distribution setting. You can import data from a spreadsheet or text file (.xls, .xlsx, .csv or .txt formats are acceptable). The Preexisting Particle Size Distribution window shown below, provides a graphical representation of the radius versus corresponding frequencies.



### System (System Definer)

Database package	Demo: Steels and Fe-alloys (FEDEMO and MFEDEMO)
Elements	Fe, C, Cr

### Conditions (Precipitation Calculator)

Composition	Fe-0.1C-12Cr Mass percent
Matrix phase	BCC_A2 All other defaults are kept.
Precipitate phases	CEMENTITE, M23C6 and M7C3

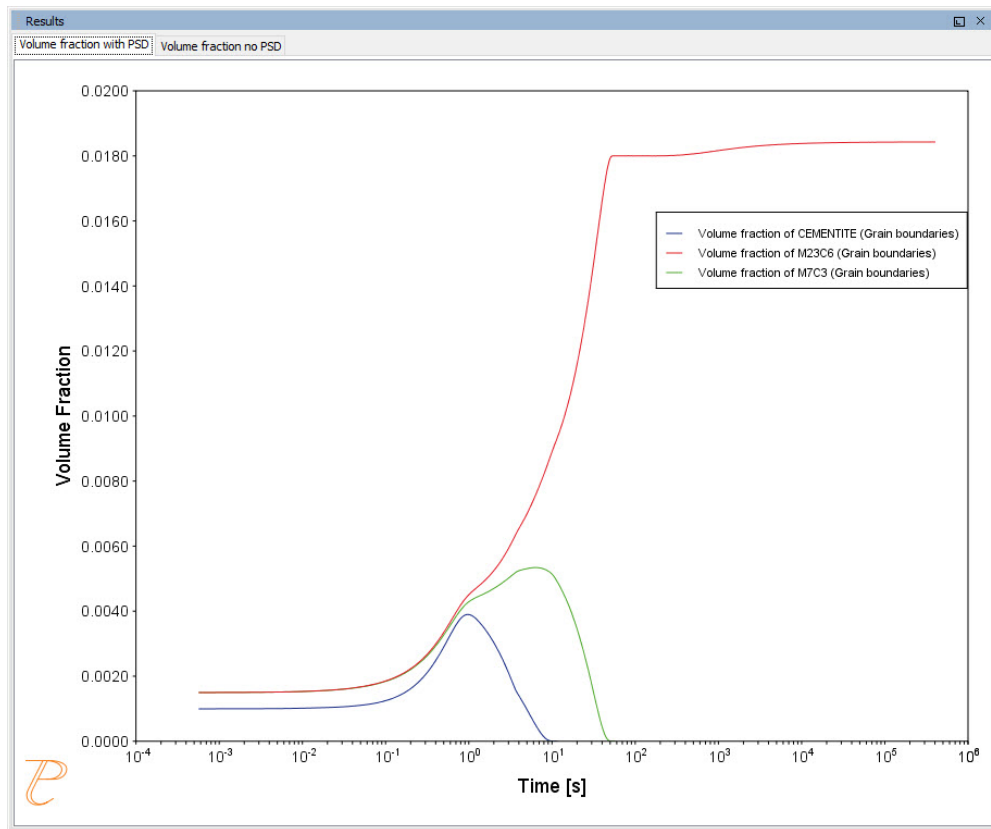
### Precipitate Phase Data Parameters (Precipitation Calculator)

Nucleation sites	Grain boundaries (all calculations): Calculated from the matrix settings with a wetting angle of 90°
Interfacial energy	User-defined function $f(r,T)$ (all calculations): <ul style="list-style-type: none"> <li>CEMENTITE: 0.167 J/m<sup>2</sup></li> </ul>

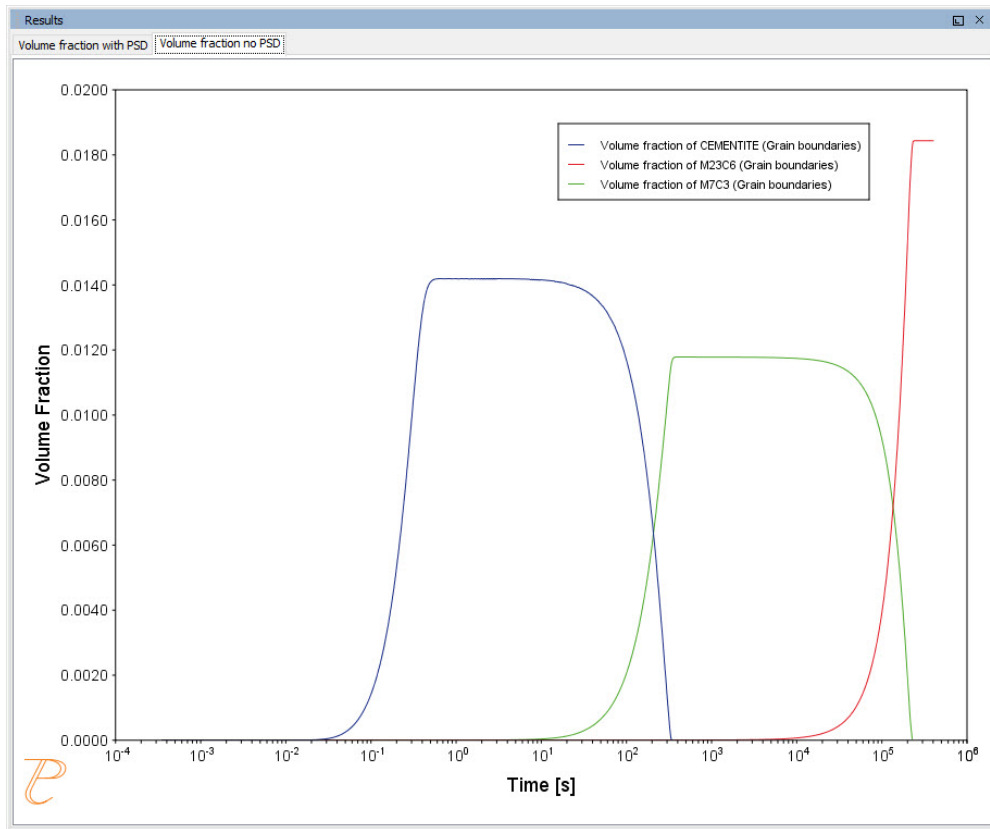
	<ul style="list-style-type: none"> <li>• M23C6 0.252 J/m<sup>2</sup></li> <li>• M7C3 0.282 J/m<sup>2</sup></li> </ul>
Preexisting size distribution (click <b>Show details</b> to display this setting)	<p>For the Precipitation Calculator including particle size distribution, and for all precipitate phases, this check box is selected.</p> <p>For each precipitate phase (CEMENTITE, M23C6 and M7C3), click <b>Edit particle size distribution</b> to make changes to the parameters. A window opens with a graphical representation of the radius vs number density.</p>
<b>Calculation Type (Precipitation Calculator)</b>	
Calculation type	Isothermal
Temperature	1053 K
Simulation time	400 000 seconds
<b>Other</b>	
File name and location	<p>Folder: Precipitation Module - TC-PRISMA</p> <p>File name: P_10_Precipitation_Initial_PSD_FeCrC.tcu</p>

## Plot Results

### Volume Fraction with Initial Particle Size Distribution



### Volume Fraction with No Initial Particle Size Distribution



### P\_11: Interfacial Energy Function

In some cases, interfacial energy may be a function of temperature or particle radius. This example uses four Precipitation Calculators at four temperature points in 30 K increments: 673 K, 703 K, 733 K, and 763 K. It is an isothermal calculation to examine the mean radius of an Al-0.12Sc system. It uses an FCC\_A1 matrix phase and AL3Sc precipitate phase with bulk nucleation sites and user-defined interfacial energy function. The user defined interfacial energy function uses an error function to set a smooth transition of the interfacial energy from 0.065 J/m<sup>2</sup> to 0.085 J/m<sup>2</sup> for particle radii below and above 1e-8m and 5e-8m, respectively.

A dataset based on Iwamura and Miura (<sup>1</sup>) data is compared with the calculated results.

#### System (System Definer)

Database package

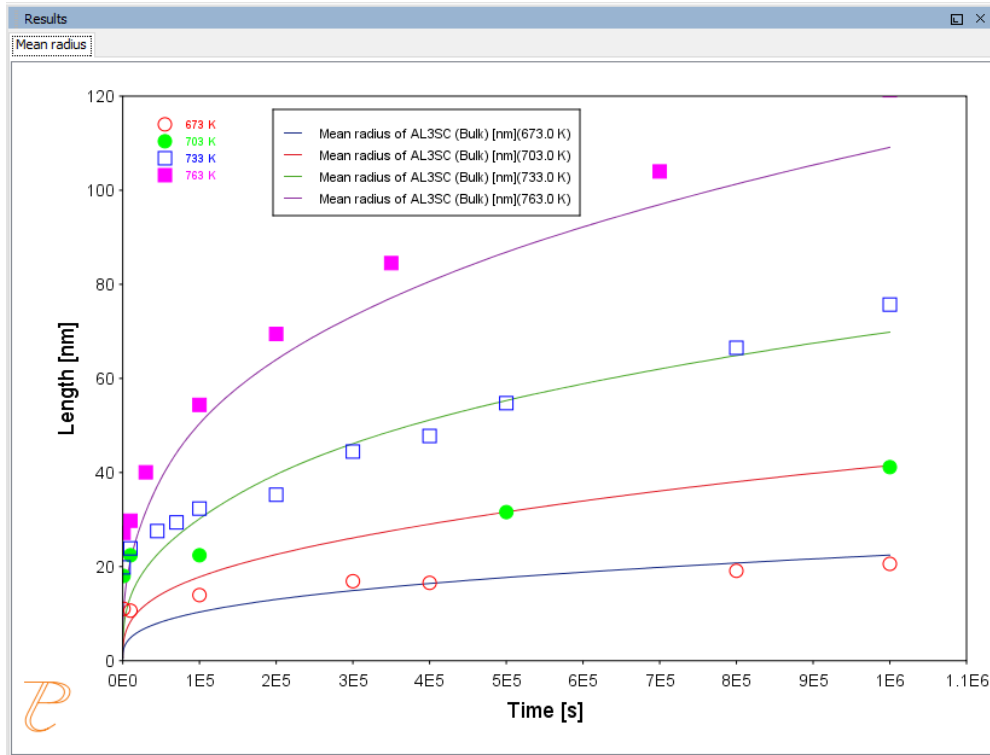
Demo: Aluminum-based Alloys (ALDEMO, MALDEMO)

<sup>1</sup>. Iwamura, S, and Y Miura. 2004. "Loss in Coherency and Coarsening Behavior of Al3Sc Precipitates." *Acta Materialia* 52 (3): 591–600.

Elements	Al, Sc
<b>Conditions (Precipitation Calculator)</b>	
Composition	Al-0.12Sc Mole percent
Matrix phase	FCC_A1 All other defaults are kept.
Precipitate phase	AL3SC Nucleation sites (all calculations): Bulk ( $6.025 \times 10^{28} \text{ m}^{-3}$ ) Interfacial energy (all calculations): User-defined function $f(r,T)$ : $0.075 + 0.011 * \text{erf}((r - 3 \times 10^{-8}) / 1 \times 10^{-8} \text{ J/m}^2)$
<b>Calculation Type (Precipitation Calculator)</b>	
Calculation type	Isothermal (all calculations)
Temperature	Four temperature points in 30 K increments: 673 K, 703 K, 733 K, and 763 K.
Simulation time	1 000 000 seconds (all calculations)
<b>Datasets (Experimental File Reader)</b>	
Wamura 2004 (Dataset 1)	Data set included with this example and imported to one Experimental File Reader.
<b>Other</b>	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_11_Interfacial_energy_function.tcu

## Plot Results

### Mean Radius



### P\_11: Interfacial Energy Function

In some cases, interfacial energy may be a function of temperature or particle radius. This example uses four Precipitation Calculators at four temperature points in 30 K increments: 673 K, 703 K, 733 K, and 763 K. It is an isothermal calculation to examine the mean radius of an Al-0.12Sc system. It uses an FCC\_A1 matrix phase and AL3SC precipitate phase with bulk nucleation sites and user-defined interfacial energy function. The user defined interfacial energy function uses an error function to set a smooth transition of the interfacial energy from 0.065 J/m<sup>2</sup> to 0.085 J/m<sup>2</sup> for particle radii below and above 1e-8m and 5e-8m, respectively.

A dataset based on Iwamura and Miura (<sup>1</sup>) data is compared with the calculated results.

#### System (System Definer)

Database package

Demo: Aluminum-based Alloys (ALDEMO, MALDEMO)

<sup>1</sup>. Iwamura, S, and Y Miura. 2004. "Loss in Coherency and Coarsening Behavior of Al3Sc Precipitates." *Acta Materialia* 52 (3): 591–600.



Elements	Al, Sc
<b>Conditions (Precipitation Calculator)</b>	
Composition	Al-0.12Sc Mole percent
Matrix phase	FCC_A1 All other defaults are kept.
Precipitate phase	AL3SC Nucleation sites (all calculations): Bulk ( $6.025 \times 10^{28} \text{ m}^{-3}$ ) Interfacial energy (all calculations): User-defined function $f(r,T)$ : $0.075 + 0.011 * \text{erf}((r - 3 \times 10^{-8}) / 1 \times 10^{-8} \text{ J/m}^2)$
<b>Calculation Type (Precipitation Calculator)</b>	
Calculation type	Isothermal (all calculations)
Temperature	Four temperature points in 30 K increments: 673 K, 703 K, 733 K, and 763 K.
Simulation time	1 000 000 seconds (all calculations)
<b>Datasets (Experimental File Reader)</b>	
Wamura 2004 (Dataset 1)	Data set included with this example and imported to one Experimental File Reader.
<b>Other</b>	
File name and location	Folder: Precipitation Module - TC-PRISMA File name: P_11_Interfacial_energy_function.tcu

## Plot Results

### Mean Radius

